IRON-POWDER and FERRITE COIL FORMS







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Iron Powder Cores

Iron Powder Cores are made in numerous shapes and sizes, such as Toroidal Cores, E-cores, Shielded Coil Forms, Sleeves etc. each of which are available in many different materials. There are two basic groups of iron powder material: (1) The Carbonyl Iron and, (2) The Hydrogen Reduced Iron.

The Carbonyl Iron cores are especially noted for their stability over a wide range of temperatures and flux levels. Their permeability range is from less than 3 mu to 35 mu and can offer excellent 'Q' factors from 50 KHz to 200 MHz. They are ideally suited for a variety of RF applications where good stability and good 'Q' are essential, also very much in demand for broadband inductors especially where high power is concerned.

The Hydrogen Reduced Iron cores have higher permeabilities ranging from 35 mu to 90 mu. Somewhat lower 'Q' can be expected from this group of cores. They are mainly used for EMI filters and low frequency chokes. They are also very much in demand for input and output filters for switched mode power supplies.

The next several pages are devoted to iron powder materials and the toroidal core configuration in particular, showing physical dimensions of available items, their $A_{\rm L}$ values and other magnetic properties, as well as how to select the proper core for your application.

In general, toroidal cores are the most efficient of any core configuration. They are highly self-shielding since most of the flux lines are contained within the core. The flux lines are essentially uniform over the entire length of the magnetic path and consequently stray magnetic fields will have very little effect on a toroidal inductor. It is seldom necessary to shield a toroidal inductor.

The A_L value of each iron powder core will be found in the charts on the next several pages. Use this A_L value and the formula found at the end of the charts to calculate the number of turns needed for your application.

Iron Powder Materials

MATERIAL #0 (u=1) Most commonly used for frequencies above 100 MHz. Available in toroidal form only. Note: Due to the nature of this material the inductance resulting from the use of the given A_L value may not be as accurate as we would like. The inductance vs. number of turns will vary greatly depending upon the winding technique.

MATERIAL #1 (u=20) A Carbonyl 'C' material very similar to material #3 except that it has higher volume resistivity and better stability. Available in toroidal form and shielded coil form.

MATERIAL #2 (u=10) A Carbonyl 'E' iron powder material having high volume resistivity. Offers high 'Q' for the 2 MHz to 30 MHz. frequency range. Available in toroidal form and shielded coil form.

MATERIAL #3 (u=35) A carbonyl 'HP' material having excellent stability and good 'Q' for the lower frequencies from 50 KHz. to 500 KHz. Available in toroidal form and shielded coil form.

MATERIAL #6 (u=8) A carbonyl 'SF' material very similar to #2 material but has an improved 'Q'. Frequency range 20 MHz to 50 MHz. Available in toroidal form and shielded coil form.

MATERIAL #10 (u=6) A powdered iron 'W' material. Offers good 'Q' and high stability for frequencies from 40 MHz to 100 MHz. Available in toroidal form and shielded coil form.

MATERIAL #12 (u=4) A synthetic oxide material which can provide good 'Q'and moderate stability for frequencies 50 MHz to 200 MHz. If high 'Q' is of prime importance this material is a good choice. If stability is of prime importance consider the #17 material. The #12 material is available in all toroidal sizes up to T-94. Not available in shielded coil form.

MATERIAL #15 (u=25) A carbonyl 'GS6' material. Has excellent stability and good 'Q'. A good choice for commercial broadcast frequencies where good 'Q' and stability are essential. Available in toroidal form only.

Material #17 (u=4) This is a new carbonyl material which is practically the same as the #12 material except that it has better temperature stability. However, as compared to the #12 material, there will be a slight $^{\circ}Q'$ loss of about 10% from 50 MHz to 100 MHz. Above 100 MHz the $^{\circ}Q'$ will slowly deteriorate up to approximately 20% lower. In toroidal form, this material is available only in sizes from T-12 through T-50. Available in all shielded coil forms.

MATERIAL #26 (u=75) A Hydrogen Reduced material. Has highest permeability of all of the iron powder materials. Used for EMI filters and DC chokes. The #26 is very similar to the older #41 material but can provide an extended frequency range. Available in Toroidal core sizes from T-30 through T-520 only.

IRON POWDER TOROIDAL CORES For Resonant Circuits

MATERIAL O Perm. 1 Freq. Range 100 MHz - 300 MHz Color -tan

Core number \/	O.D. (inches)	I.D. (inches)	Hgt. (inches)	$\frac{1}{(cm)}$	$A_{\rm e} ({ m cm})^2$	$V_{\mathbf{e}} \atop (\mathbf{cm})^3$	A _L Value uh/100 turns
T-12-0	.125	.062	.050	0.74	.010	.007	3.0
T-16-0	.160	.078	.060	0.95	.016	.015	3.0
T-20-0	.200	.088	.070	1.15	.025	.029	3.5
T-25-0	.255	.120	.096	1.50	.042	.063	4.5
T-30-0	.307	.151	.128	1.83	.065	.119	6.0
T-37-0	.375	.205	.128	2.32	.070	.162	4.9
T-44-0	.440	.229	.159	2.67	.107	.286	6.5
T-50-0	.500	.303	.190	3.03	.121	.367	6.4
T-68-0	.690	.370	.190	4.24	.196	.831	7.5
T-80-0	.795	. 495	.250	5.15	.242	1.246	8.5
T-94-0	.942	.560	.312	6.00	.385	2.310	10.6
T-106-0	1.060	.570	.437	6.50	.690	4.485	19.0
T-130-0	1.300	.780	.437	8.29	.730	6.052	15.0

Due to the nature of the `0' material, the inductance may vary greatly depending upon your winding technique. This may cause some discrepancy between calculated and measured inductance.

MATERIAL 1 Perm 20 Freq. Range 0.5 MHz- 5. MHz Color -	MATERIAL	1	Perm 20	Frea.	Range	0.5	MHz-	5.	MHz	Color -	Blue
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Core number	0.D. (inches)	I.D. (inches)	Hgt. (inches)	1 _e (cm)	${\rm A_e} \over {\rm (cm)}^2$	$(cm)^3$	A _L Value uh/100 turns
\/ T-12-1	.125	.062	.050	0.74	.010	.007	48
T-16-1	.160	.078	.060	0.95	.016	.015	44
T-20-1	.200	.088	.070	1.15	.025	.029	52
T-25-1	.255	.120	.096	1.50	.042	.063	70
T-30-1	.307	.151	.128	1.83	.065	.119	85
T-37-1	.375	.205	.128	2.32	.070	.162	80
T-44-1	.440	.229	.159	2.67	.107	.286	105
T-50-1	.500	.303	.190	3.03	.121	.367	100
T-68-1	.690	.370	.190	4.24	.196	.831	115
T-80-1	.795	.495	.250	5.15	.242	1.246	115
T-94-1	.942	.560	.312	6.00	.385	2.310	160
T-106-1	1.060	.570	.437	6.50	.690	4.485	325
T-130-1	1.300	.780	.437	8.29	.730	6.052	200
T-157-1	1.570	.950	.570	10.05	1.140	11.457	320
T-184-1	1.840	.950	.710	11.12	2.040	22.685	500
T-200-1	2.000	1.250	.550	12.97	1.330	17.250	250

Note: Most cores can be very useful well below the lower frequency limit shown above.

IRON POWDER TOROIDAL CORES For Resonant Circuits

MATERI	AL 2	Perm.	10 Freq	Range	2 MHz - 3	0 MHz Colo	r Red
Core	O.D.	I.D.	Hgt.	I_e	A	V _e	A _{r.} Value
number \/	(inches)	(inches)	(inches)	(cm)	$\frac{A_e}{(cm)^2}$	$\frac{V_{e}}{(cm)^3}$	uh/100 turns
T-12-2	.125	.062	.050	0.74	.010	.007	20
T-16-2	.160	.078	.060	0.95	.016	.015	22
T-20-2	.200	.088	.070	1.15	.025	.029	25
T-25-2	.255	.120	.096	1.50	.042	.063	34
T-30-2	.307	.151	.128	1.83	.065	.119	43
T-37-2	.375	.205	.128	2.32	.070	.162	40
T-44-2	.440	.229	.159	2.67	.107	.286	52
T-50-2	.500	.303	.190	3.03	.121	.367	49
T-68-2	.690	.370	.190	4.24	.196	.831	57
T-80-2	.795	.495	.250	5.15	.242	1.246	55
T-94-2	.942	.560	.312	6.00	.385	2.310	84
T-106-2	1.060	.570	.437	6.50	.690	4.485	135
T-130-2	1.300	.780	.437	8.29	.730	6.052	110
T-157-2	1.570	.950	.570	10.05	1.140	11.457	140
T-184-2	1.840	.950	.710	11.12	2.040	22.685	240
T-200-2	2.000	1.250	.550	12.97	1.330	17.250	120
T-200A-2	2.000	1.250	1.000	12.97	2.240	29.050	218
T-225 -2	2.250	1.405	.550	14.56	1.508	21.956	120
T-225A-2	2.250	1.485	1.000	14.56	2.730	39.749	215
T-300 -2	3.058	1.925	.500	19.83	1.810	35.892	114
T-300A-2	3.048	1.925	1.000	19.83	3.580	70.991	228
T-400 -2	4.000	2.250	.650	24.93	3.660	91.244	180
T-400A-2	4.000	2.250	1.300	24.93	7.432	185.280	360
T-520 -2	5.200	3.080	.800	33.16	5.460	181.000	207

MATERI	AL 3	Perm 35	Freq.	Range .05 !	MHz - 5. N	MHz Colo	or - Gray
Core number \/	O.D. (inches)	I.D. (inches)	Hgt. (inches)	I _e (cm)	A _e (cm) ²	V _e (cm) ³	A _L Value uh/100 turns
T-12-3	.125	.062	.050	0.74	.010	.007	60
T-16-3	.160	.078	.060	0.95	.016	.015	61
T-20-3	.200	.088	.070	1.15	.025	.029	76
T-25-3	.255	.120	.096	1.50	.042	.063	100
T-30-3	.307	.151	.128	1.83	.065	.119	140
T-37-3	.375	.205	.128	2.32	.070	.162	120
T-44-3	.440	.229	.159	2.67	.107	.286	180
T-50-3	.500	.303	.190	3.03	.121	.367	175
T-68-3	.690	.370	.190	4.24	.196	.831	195
T-80-3	.795	.495	.250	5.15	.242	1.246	180
T-94-3	.942	.560	.312	6.00	.385	2.310	248
T-106-3	1.060	.570	.437	6.50	.690	4.485	450
T-130-3	1.300	.780	.437	8.29	.730	6.052	350
T-157-3	1.570	.950	.570	10.05	1.140	11.457	420
T-184-3	1.840	.950	.710	11.12	2.040	22.685	720
T-200-3	2.000	1.250	.550	12.97	1.330	17.250	425
T-200A-3	2.000	1.250	1.000	12.97	2.240	29.050	460
T-225 -3	2.250	1.405	.550	14.56	1.508	21.956	425

IRON POWDER TOROIDAL CORES For Resonant Circuits

MATERIAL 6 Perm. 8 Freq. Range 10 MHz - 50 MHz Color - Yellow

Core number	O.D. (inches)	I.D. (inches)	Hgt. (inches)	1 _e (cm)	A _e (cm) ²	$V_{\mathbf{e}}$ $(\mathbf{cm})^3$	A _L Value uh/100 turns
T-12-6	.125	.062	.050	0.74	.010	.007	17
T-16-6	.160	.078	.060	0.95	.016	.015	19
T-20-6	.200	.088	.070	1.15	.025	.029	22
T-25-6	.255	.120	.096	1.50	.042	.063	27
T-30-6	.307	.151	.128	1.83	.065	.119	36
T-37-6	.375	.205	.128	2.32	.070	.162	30
T-44-6	.440	.229	.159	2.67	.107	.286	42
T-50-6	.500	.303	.190	3.03	.121	.367	46
T-68-6	.690	.370	.190	4.24	.196	.831	47
T-80-6	.795	. 495	.250	5.15	.242	1.246	45
T-94-6	.942	.560	.312	6.00	.385	2.310	70
T-106-6	1.060	.570	.437	6.50	.690	4.485	116
T-130-6	1.300	.780	.437	8.29	.730	6.052	96
T-157-6	1.570	.950	.570	10.05	1.140	11.457	115
T-184-6	1.840	.950	.710	11.12	2.040	22.685	195
T-200-6	2.000	1.250	.550	12.97	1.330	17.250	100
T-200A-6	2.000	1.250	1.000	12.97	2.240	29.050	180
T-225 -6	2.250	1.405	.550	14.56	1.508	21.956	100

MATERIAL 7 Perm 9 Freq. Range 3 MHz - 35 Mhz. Color - White

Core number	O.D.	I.D.	Hgt. (inches)	1 _e	A _e (cm) ²	V _e (cm) ³	A _L Value
\/	(Inches)	(Inches)	(Inches)	(cm)	(CM)	(CIII)	uh/100 turns
T-25-7	.255	.120	.096	1.50	.042	.063	29
T-37-7	.375	.205	.128	2.32	.070	.162	32
T-50-7	.500	.303	.190	3.03	.121	.367	43
T-68-7	.690	.370	.190	4.24	.196	.831	52

MATERIAL 10 Perm 6 Freq. Range 30 MHz - 100 MHz Color - Black

Core number \/	O.D. (inches)	I.D. (inches)	Hgt. (inches)	$\frac{1}{e}$ (cm)	A _e (cm) ²	$V_{\mathbf{e}}$	A _L Value uh/100 turns
T-12-10	.125	.062	.050	0.74	.010	.007	12
T-16-10	.160	.078	.060	0.95	.016	.015	13
T-20-10	.200	.088	.070	1.15	.025	.029	16
T-25-10	.255	.120	.096	1.50	.042	.063	19
T-30-10	.307	.151	.128	1.83	.065	.119	25
T-37-10	.375	.205	.128	2.32	.070	.162	25
T-44-10	.440	.229	.159	2.67	.107	.286	33
T-50-10	.500	.303	.190	3.03	.121	.367	31
T-68-10	.690	.370	.190	4.24	.196	.831	32
T-80-10	.795	.495	.250	5.15	.242	1.246	32
T-94-10	.942	.560	.312	6.00	.385	2.310	58

IRON POWDER TOROIDAL CORES For Resonant Circuits

MATERIAL 12 Perm 4 Freq. range 50 MHz - 200 MHz. Grn & Wh.

Core number	O.D. (inches)	I.D. (inches)	Hgt. (inches)	$\frac{\mathrm{I}_{\mathrm{e}}}{\mathrm{(cm)}}$	$\frac{A_e}{(cm)^2}$	V _e (cm) ³	A _L Value uh/100 turns
\/	105	060	050		010	207	
T-12-12	.125	.062	.050	0.74	.010	.007	7.5
T-16-12	.160	.078	.060	0.95	.016	.015	8.0
T-20-12	.200	.088	.070	1.15	.025	.029	10.0
T-25-12	.255	.120	.096	1.50	.042	.063	12.0
T-30-12	.307	.151	.128	1.83	.065	.119	16.0
T-37-12	.375	.205	.128	2.32	.070	.162	15.0
T-44-12	.440	.229	.159	2.67	.107	.286	18.5
T-50-12	.500	.303	.190	3.03	.121	.367	18.0
T-68-12	.690	.370	.190	4.24	.196	.831	21.0
T-80-12	.795	.495	.250	5.15	.242	1.246	22.0
T-94-12	.942	.560	.312	6.00	.385	2.310	32.0

Note: If greater stability is desired ask for #17 material, but 'Q' will be sacrificed. See material description and temperature chart. Sizes available only T-12 through T-50. Color code for material #17 - Blue and Yellow.

MATER	RIAL	15	Perm	n 25	Freq. 0.1	MHz - 2.	MHz C	olor - Rd & Wh
Core	O.D.	Ι.	D.	Hgt.	$I_{\mathbf{e}}$	A _e 2	V_	A _{I.} Value
number	(inches)	(inc	hes)	(inches)		(cm) ²	V _e (cm) ³	uh/100 turns
\/								
T-12-15	.125	.0	162	.050	0.74	.010	.007	50
T-16-15	.160	.0	178	.060	0.95	.016	.015	55
T-20-15	.200		88	.070	1.15	.025	.029	65
T-25-15	.255	.1	20	.096	1.50	.042	.063	85
T-30-15	.307	. 1	.51	.128	1.83	.065	.119	93
T-37-15	.375	.2	:05	.128	2.32	.070	.162	90
T-44-15	.440	. 2	29	.159	2.67	.107	. 286	160
T-50-15	.500	.3	03	.190	3.03	.121	.367	135
T-68-15	.690	.3	70	.190	4.24	.196	.831	180
T-80-15	.795	.4	95	.250	5.15	.242	1.246	170
T-94-15	.942	.5	60	.312	6.00	.385	2.310	200
T-106-15	1.060	.5	70	.437	6.50	.690	4.485	345
T-130-15	1.300	.7	80	.437	8.29	.730	6.052	250
T-157-15	1.570	.9	50	.570	10.05	1.140	11.457	<u>36</u> 0

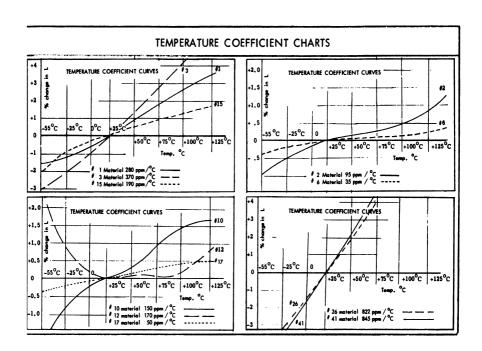
MATERIAL 26 See AC Line Filter and DC Choke section.

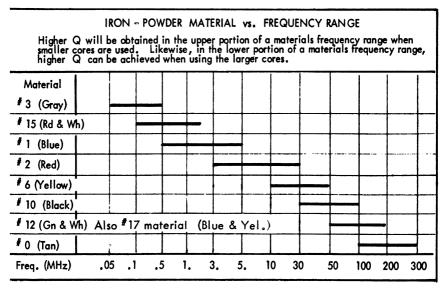
The following equations are useful for calculating number of turns, inductance or the A_L value of any Iron Powder toroidal core. Each core has been assigned an A_L value which will be found in the preceding Iron Powder toroidal core charts.

$$N = 100 \sqrt{\frac{\text{desired 'L' (uh)}}{A_L \text{ (uh/100 turns)}}} \qquad \qquad L \text{ (uh)} = \frac{A_L \times N^2}{10,000} \qquad \qquad A_L \text{ (uh/100 turns)} = \frac{10,000 \times \text{'L' (uh)}}{N^2}$$

N = number of turns: L = inductance (uh) A_L = inductance index (uh / 100 turns

Iron Powder Toroidal Cores





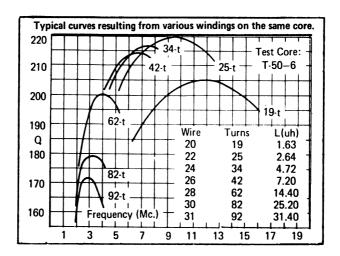
IRON POWDER TOROIDAL CORES

			F	hys	ica1	Dimensions						
Core Size	Outer diam. (in)	Inner diam. (in)	Height	Mean lgth. (cm)	Cross sect. (cm ²)	1	Core Size	Outer diam (in)	Inner diam (in)	Height (in)	Mean lgth. (cm)	Cross sect. (cm ²)
T- 12	.125	.062	.050	0.75	.010		T-130	1.30	.78	.437	8.29	0.73
T- 16	.160	.078	.060	0.95	.016		T-157	1.57	.95	.570	10.05	1.14
T- 20	.200	.088	.070	1.15	.025		T-184	1.84	.95	.710	11.12	2.04
T- 25	.250	.120	.096	1.50	.042		T-200	2.00	1.25	.550	12.97	1.33
T- 30	.307	.151	.128	1.83	.065		T-200A	2.00	1.25	1.000	12.97	2.42
T- 37	.375	.205	.128	2.32	.070		T-225	2.25	1.40	.550	14.56	1.50
T- 44	.440	.229	.159	2.67	.107		T-225A	2.25	1.40	1.000	14.56	2.73
T- 50	.500	.300	.190	3.20	.121		T-300	3.00	1.92	.500	19.83	1.81
T- 68	.690	.370	.190	4.24	.196		T-300A	3.00	1.92	1.000	19.83	3.58
T- 80	.795	.495	.250	5.15	.242		T-400	4.00	2.25	.650	24.93	3.66
T- 94	.942	.560	.312	6.00	.385		T-400A	4.00	2.25	1.000	24.93	7.43
T-106	1.060	.570	.437	6.50	.690		T-500	5.20	3.08	.800	33.16	5.46

					0.341	c 141	10 Mix	12 Mix	0 Mix
Core	26 Mix	3 Mix	15 Mix	1 Mix Blue	2 Mix Red	6 Mix Yellow	Black	Grn-Wh	Tan
Size	Yel-Wh	Gray u = 35	Rd-Wh $u = 25$	u = 20	u = 10	u = 8	u = 6	u = 4	u = 1
\/	u = 75 Ihz> Pwr Frq	.05 -0.5	0.1 - 2.	0.5 - 5.	2 - 30	10 - 50	30-100	50-200	100-30
Γ- 12-	na	60	50	48	20	17	12	7.5	3.0
Γ- 16-	145	61	55	44	22	19	13	8 0	3.0
r- 20-	180	76	65	52	27	22	16	10.0	3.5
Γ- 25-	235	100	85	70	34	27	19	12.0	4.5
r- 30-	325	140	93	85	43	36	25	16.0	6.0
r- 37-	. 275	120	90	80	40	30	25	15.0	4.9
Γ- 44-	360	180	160	105	52	42	33	18.5	6.5
r- 50-	320	175	135	100	49	40	31	18.0	6.4
r- 68-	420	195	180	115	57	47	32	21.0	7.5
r- 80-	450	180	170	115	55	45	32	22.0	8.5
T- 94-	590	248	200	160	84	70	58	32.0	10.6
r-106-	900	450	345	325	135	116	na	na	19.0
Γ-130-	785	350	250	200	110	96	na	na	15.0
T-157-	970	420	360	320	140	115	na	na	na
T-184-	1640	720	na	500	240	195	na	na	na
T-200-	895	425	na	250	120	100	na	na	na
T-200A-	1550	760	na	na	218	180	na	na	na
T-225-	950	424	na	na	120	100	na	na	na
T-225A-	1600	na	na	na	215	na	na	na	na
T-300-	800	na	na	na	114	na	na	na	na
T-300A-	1600	na	na	na	228	na	na	na	na
T-400-	1300	na	na	na	185	na	na	na	na
T-400A-	2600	na	na	na	360	na	na	na	na
T-500-	1460	na	na	na	207	na	na	na	na

IRON-POWDER TOROIDAL CORES

TYPICAL 'Q' CURVES various windings, same core



The above chart shows typical curves resulting from a number of various windings on the same core. The test core was a T-50-6.

The following pages contain a number of curves which were measured and plotted from actual windings, therefore there may be a slight variation from a mathematical calculation.

IRON POWDER TOROIDAL CORES

'Q' vs. Frequency 100 KHz - 30 MHz

All coils are single layer magnetic wire, not necessarily optimum values.

	MI	X-3		Q vs Frequency Mix-3	_
T130-3* T106-3 T94-3 T80-3 T68-3 T50-3 T44-3 T37-3* T30-3*	Turns 200 100 100 100 100 100 100 100	Wire #28 #26 #28 #30 #32 #34 #33	L (uh) 1400 450 248 180 195 175 180 120	150 1106-3 194-3 150-3 150-3 125-3 125-3	
T25-3*	100	#34	100	50 T20-3	
T20-3* *Not Sing	100 le Layers	#38	76	100 150 200 300 400 500 600 800 1000 Frequency (KHz)	_
	МІ	X-2		250 Q vs Frequency T94-2 Q vs Frequency Mix-2	
T 94-2 T 80-2 T 68-2 T 50-2 T 44-2 T 30-2 T 30-2 T 25-2 T 20-2 T 10-2	Turns 100 100 100 77 66 53 47 30 30 25	Wire #28 #30 #30 #30 #32 #33 #34 #40	L (uh) 84 55 57 29 23 11.5 9.3 3.0 2.4 1.3	T682 T50.2 T442 T37.2 T30.2 T100 T10.2 T10	
	MI	X-6		250 T80-6 Q vs Frequency Mix-6	
T 80-6 T 68-6 T 50-6 T 44-6 T 37-6 T 30-6 T 27-6 T 25-6 T 20-6 T 16-6	Turns 70 60 50 47 40 37 32 30 30 25	Wire #26 #27 #27 #28 #30 #30 #30 #33 #33	L (uh) 22 17 10 9.3 4.8 4.9 2.8 2.5 2.0 1.2	200 T50-6 T44-6 T37-6 T30-6 T30-6 T30-6 T27-6 T20-6 T10-6 T1	

20

Frequency (MHz)

30

T 12-6

T 10-6

22

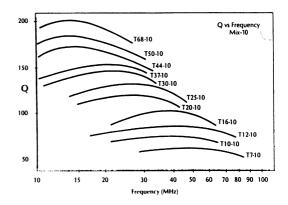
#34

IRON POWDER TOROIDAL CORES

'Q' vs. Frequency 10 MHz - 200 MHz

All coils are single layer magnetic wire, not necessarily optimum values.

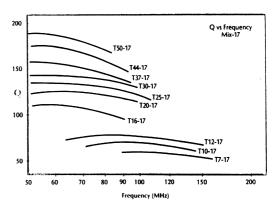
	MI	X-10	
	Turns	Wire	L (uh)
68-10	15	#20	.80
50-10	14	#20	.70
44-10	13	#20	.65
37-10	12	#20	.40
30-10	14	#24	.55
25-10	14	#26	.45
20-10	13	#27	.30
16-10	11	#27	.20
12-10	10	#29	.15
10-10	10	#32	.10
7-10	10	#36	.10



MIX-17

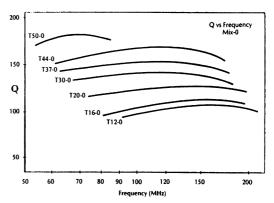
	Turns	Wire	L (uh)
50-17	9	#20	.14
44-17	7	#20	.13
37-17	8	#20	.12
30-17	8	#22	.13
25-17	9	#24	.12
20-17	9	#26	.10
16-17	9	#28	.08
12-17	9	#30	.08
10-17	7	#32	.07
7-17	7	#35	.05

)TE: Mix 12 will yield slightly higher Q than Mix 17 but is not recommended for applications requiring good stability.



MIX-0

	Turns	Wire	L (uh)
50-0	10	#20	.12
44-0	8	#20	.08
37-0	8	#22	.07
30-0	8	#22	.07
20-0	8	#24	.06
16-0	7	#26	.04
12-0	7	#26	.03



INDUCTANCE CHARTS

Iron Powder Toroids

	IRON POWDER TOROIDAL CORES													
MATERIA	MATERIAL #0 Inductance (uh) vs. Size, Material and Number of Turns													
Turns>	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size T-106 T-94 T-80 T-68 T-50	.19 .10 .08 .07	.76 .40 .34 .30	1.7 .90 .77 .67	3.0 1.7 1.4 1.2 1.0	4.8 2.7 2.1 1.9	6.8 3.8 3.0 2.7 2.3	9.3 5.2 4.2 3.7 3.1	12 6.8 5.4 4.8 4.1	15 8.6 6.9 6.0	19 10. 8.5 7.5	23 13 10 -	27 15 12 -	32 18 14 -	37 21 - -
T-37 T-25	.05	.20	.44 .41	.7 -	1.2	-	-	-	-	-	-	-	-	- -
T-20 T-16	.03	.14	-	-	-	- -	-	-	-	- -	-	-	-	-
T-12	.03	-		-	-	-	-	-	-	-	_	-	-	

				IR	ON PO	WDER	TOROI	DAL C	ORES					
MATERI	MATERIAL #1 Inductance (uh) vs.									rial	and N	umber	of T	urns
Turns	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size T-106 T-94 T-80 T-68 T-50 T-37 T-25 T-20 T-16 T-12	3.2 1.6 1.2 1.2 1.0 .8 .7 .5 .4	13 6.4 4.6 4.6 4.0 3.2 2.8 2.0 1.7	29 14 10 10 9 7 6	52 25 18 18 16 13 -	81 40 28 28 25 20 - - -	117 57 41 41 36 - - -	159 78 56 56 49 - - -	208 102 73 73 64 - -	263 130 93 93 - - - -	325 160 115 115 - - - -	393 194 139 139 - - - -	468 230 166 166 - - - -	549 270 194 194 - - - -	637 304 - - - - - - -

				IRON	POWD	ER TO	OROID	AL C	ORES		-			
MATERIA	MATERIAL # 2 Inductance (uh) vs. Size, Material and Number of Turns													
Turns>	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size														
T-106	1.4	5	12	22	34	49	66	86	109	135	163	194	228	265
T-94	.8	3	8	13	21	30	41	54	68	84	101	120	131	142
T-80	.6	2	5	9	14	20	27	35	45	55	66	79	93	-
T-68	.6	2	5	9	15	21	29	38	48	59	-	l -	-	-
T-50	.5	2	2	8	12	18	24	31	l -	l -	l -	۱ -	-	-
T-37	.4	2	4	6	10	-	- 1	-	-	l -	-	-	-	-
T-25	.3	1	3	-	-	۱ -	l	-	l -	l -	l -	l -	-	-
T-20	.3	1	- 1	- 1	-	-	-	-	-	-	1 -	l -	-	-
T-16	.2	-	-	-	-	-	- 1	-	-	-	-	-	-	-
T-12	.1	-	-	-	-	-	-	-	-	-	-	-	-	-

INDUCTANCE CHARTS

Iron Powder Toroids

				IR	ON PO	WDER	TOROI	DAL C	ORES					
MATERIA	MATERIAL #3 Inductance (uh) vs. Size, Material and Number of Turns													
Turns>	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size T-106 T-94 T-80 T-68 T-50 T-37 T-25 T-20 T-16	5 2 2 3 2 1 1 .9	18 10 7 8 7 5 4 4	41 22 16 18 16 9	72 40 29 31 26 -	113 62 45 49 44 - -	182 89 65 70 63 - -	221 121 88 96 86 -	288 159 115 125 112 - -	365 200 146 158 - - -	450 248 180 185 - -	545 300 218 - - -	648 357 259 - - - -	761 419 304 - - - -	882 486 - - - - -
T-12	.6	-	-	-	-	-	-	-	-	-	-	-	-	-

		IRON POWDER TOROIDAL CORES												
MATERIA	L #6		In	ductai	nce (1	uh)	vs.	Size,	Mate	rial	and N	umber	of T	urns
Turns>	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size T-106 T-94 T-80 T-68 T-50 T-37	1.1 .7 .5 .5 .4 .4	5 3 2 2 2 1 1	10 6 4 4 3 3	19 11 7 7 6 5	30 18 11 11 10 7	42 25 16 17 14 -	57 34 22 23 20 -	74 45 29 30 26 -	94 57 36 38 - -	116 70 45 47 - -	140 85 54 - - -	167 100 64 - - -	196 118 76 - - -	227 137 - - - - -
T-20 T-16	.2	.8	1 -	-	-	-	-	-	-	-	-	-	<u>-</u>	-
T-12	.1	•	-	-	-	-	-	-	-	-	-	-	-	-

	IRON POWDER TOROIDAL CORES													
MATERIAL #10 Inductance (uh) vs. Size, Material and Number of Turn												urns		
Turns>	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size> T-94 T-80 T-68	.6 .3	2 1 1	5 3 2	9 5 5	15 8 8	21 12 12	28 16 16	37 21 20	47 27 26	58 33 32	70 40 -	84 48 -	98 54 -	113 - -
T-50 T-37	.3	1	3 2	5 4	8 6	11	15	20	-	-	-	-	-	-
T-25	.2	.8	2	-	-	-	-	-	-	-	-	-	-	-
T-20 T-16	.1	.6 .5	-	-	-	-	-	-	-	-	-	-	-	-
T-12	.1		-	-	-	-	-	-	-	-	-	-	-	-

INDUCTANCE CHARTS

Iron Powder Toroids

				IRON	POWD	ER TO	ROIDA	L COR	ES					
MATERIAL #15 Inductance (uh) vs. Size, Material and Number of Turr											urns			
Turns	10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size T-106 T-94 T-80 T-68 T-50 T-37 T-25 T-20 T-16 T-12	4 2 2 2 1 1 1 .5 .5	14 8 7 7 5 4 3 3	31 18 15 16 12 8 8	55 32 27 29 22 14 - -	86 50 43 45 34 23 - -	124 72 61 65 49 - - -	169 98 83 88 66 - - -	221 128 109 115 86 - - -	279 162 138 146 - - - -	345 200 170 180 - - - -	417 242 206 - - - - - -	497 288 245 - - - - - -	583 338 287 - - - - - -	676 392 - - - - - - -

	IRON POWDER TOROIDAL CORES													
MATER	MATERIAL #17 Inductance (uh) vs. Size, Material and Number of Turns													
Turns	> 10	20	30	40	50	60	70	80	90	100	110	120	130	140
Size T-94 T-80 T-68 T-50 T-37 T-25 T-20 T-16 T-12	.3 .2 .2 .2 .1 .1 .08	1 .8 .8 .7 .6 .5 .4	3 2 2 2 1 1 -	5 4 3 3 2 - - -	8 6 5 4 - -	12 6 7 7 - - -	16 11 10 9 - - -	20 14 13 12 - - -	30 18 17 - - - -	32 22 21 - - - -	39 27 - - - - -	46 32 - - - - -	54 37 - - - - -	63

				IRON	POWD	ER T	OROID	AL C	ORES					
MATERIA	AL #2	26	Ind	ducta	nce (uh) '	vs.	Size,	Mate	rial	and I	Number	of T	lurns
Turns>	10	20	30	40	50	60	70	80	.90	100	110	120	130	140
Size														
T-106	9	36	81	144	245	324	441	576	729	900	089	1296	1521	1764
T-94	6	24	53	94	148	212	289	378	478	590	714	850	997	1156
T-80	5	18	41	72	113	162	221	288	365	450	545	648	761	882
T-68	4	17	38	67	105	151	206	269	340	420	508	605	710	823
T-50	3	13	29	51	80	115	157	205	259	320	387	461	541	627
T-37	2.7	11	25	44	69	135	176	223	-	-	-	-	-	-

INDUCTANCE CHART Iron Powder Toroids

Inductance (uh) vs. Size, Material and Number of Turns

Turns>	10	20	30	40	50	60	70	80	90	100	110	120	130
Core Numbe	r												
T-520-26	15	58	131	233	365	526	715	934	1182	1460	1767	2102	2/67
T-520-2	2	8	18	33	51	74	101	132	167				
T-400A-26	26	104	324	416	650	936	1274	1664	2106	2600	3146	3744	4394
T-400A-2	4	14	32	57	90	130	176	230	292				608
T-400-26	13	53	119	211	330	475	646				1597		2231
T-400-2	2	7	17	27	46	67	91	118	150			266	313
T-300A-26	16	64	144	256	400	576							
T-300A-2	2	9	20	36	57	82	784 118	1024 146	1296 185	228		2304 328	385
T-300-26	8	33	74	132	06	297							
T-300-2	1	5	10	132	29	41	404 56	528 74	668 93	825 115	998 139	188 166	1394 194
T-225A-26	16	64											
T-225A-2	2	9	144 19	256 34	400 54	576 77	784 105	1024 138	1296 174	1600 215		2304	
T-225-26		-									276	310	385
T-225-26	10 1	38 5	86 11	152 19	238	342 43	466 59	608 79	770		1150		1607
T-225-3	4	17	38	68	106	153	208	272	97 344	120 425	145 514	173 612	203
T-225-6	1	4	9	16	25	36	49	64	81	100	121	144	718 169
T-200A-26	16	62	136	248	388	558	760	992					
T-200A-1	5	18	41	73	114	164	223	291	1256 369	455	1875	2418	2619
T-200A-2	2	9	19	35	55	78	107	140	177	218	551 264	655 314	764
T-200A-3	5	18	41	74	115	165	225	294	373	460	557	662	368 777
T-200A-6	2	7	16	29	45	65	88	115	146	180	218	259	304
T-200-26	9	36	81	143	224	322	439	573	725	895			
T-200-1	3	10	23	40	63	90	123	160	203	250	1082 303	1289 360	1513 423
T-200-2	1	5	11	19	30	43	59	79	97	120	145	173	203
T-200-3	4	17	38	68	106	153	208	272	344	425	514	612	718
T-200-6	1	4	9	16	25	36	49	64	81	100	121	144	169
T-184-26	16	66	148	262	410	590	804	1049	1320	1640	1984	2362	
T-184-1	5	20	45	80	125	180	245	320	405	500	605	720	845
T-184-2	2	10	22	38	60	86	118	154	194	240	290	396	406
T-184-3	7	29	65	115	180	259	353	461	583	720	871		1217
T-184-6	2	8	18	31	49	70	96	125	158	195	236	281	330
T-157-26	10	34	87	155	243	349	475	621	786	970	1174	1397	1630
T-157-1	3	13	29	51	80	115	157	205	259	320	387	461	541
T-157-2	1	6	13	22	35	50	69	90	113	140	169	202	237
T-157-3	4	17	38	67	105	151	206	269	340	420	508	605	710
T-157-6	1	5	10	18	29	41	56	74	93	115	139	166	194
T-157-15	4	14	32	58	90	130	176	230	292	360	436	518	608
T-130-26	8	31	71	126	196	283	385	502	636	785	950	1130	1327
T-130-1	2	8	18	32	50	72	98	128	162	200	242	288	334
T-130-2	1	4	10	18	28	40	54	70	89	110	133	158	186
T-130-3	4	13	36	56	88	127	172	224	284	350	424	504	592
T-130-6	1	4	9	15	24	35	47	61	78	96	116	138	162
T-130-15	3	10	23	40	63	90	123	160	203	250	303	360	423

		Coppe	r Wire	Table	e	
Wire size AWG	Diameter in inches (enamel)	Circular mil area	Turns per linear inch	Turns per sq.cm	Contineous duty current (amps) single wire,open air	
8 10 12	.1285 .1019 .0808	16510 10380 6530	7.6 10.7 12.0	13.8 21.7	73 55 41	46 33 23
14 16 18	.0640 .0508 .0403	4107 2583 1624	15.0 18.9 23.6	34.1 61.2 79.1	32 22 16	17 13 10
20 22 24	.0319 .0253 .0201	1022 642 404	29.4 37.0 46.3	124.0 186.0 294.0	11 	7.5 5.0
26 28 30	.0159 .0126 .0100	254 160 101	58.0 72.7 90.5	465.0 728.0 1085.0	 	
32 34 36	.0079 .0063 .0050	63 40 25	113.0 141.0 175.0	1628.0 2480.0 3876.0	 	
38 40	.0039	16 10	224.0 382.0	5736.0 10077.0		

Iron	Ро	wd App									ns ingle	& layer	Win		Si	ze
Wire Sz.	10	12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
Core\/No																
T-12	0	0	0	1	1	1	2	4	5	8	11	15	21	29	37	47
T-16	0	0	1	1	1	3	3	5	8	11	16	21	29	38	49	63
T-20	0	1	1	1	3	4	5	6	9	14	18	25	33	43	56	72
T-25	1	1	1	3	4	5	7	11	15	21	28	37	48	62	79	101
T-30	1	1	3	4	5	7	11	15	21	28	37	48	62	78	101	129
T-37	1	3	5	7	9	12	17	23	31	41	53	67	87	110	140	177
T-44	3	5	6	7	10	15	20	27	35	46	60	76	97	124	157	199
T-50	5	6	8	11	16	21	28	37	49	63	81	103	131	166	210	265
T-68	7	9	12	15	21	28	36	47	61	79	101	127	162	205	257	325
T-80	8	12	17	23	30	39	51	66	84	108	137	172	219	276	347	438
T-94	10	14	20	27	35	45	58	75	96	123	156	195	248	313	393	496
T-106	10	14	20	27	35	45	58	75	96	123	156	195	248	313	393	496
T-130	17	23	30	40	51	66	83	107	137	173	220	275	348	439	550	693
T-157	22	29	38	50	64	82	104	132	168	213	270	336	426	536	672	846
T-184	22	29	38	50	64	82	104	132	168	213	270	336	426	536	672	846
T-200	31	41	53	68	86	109	139	176	223	282	357	445	562	707	886	111.
T-225	36	46	60	77	98	123	156	198	250	317	400	499	631	793	993	1250
T-300	52	66	85	108	137	172	217	274	347	438	553	688	870	1093	1368	172
T-400 T-520	61 86	79 110	100 149	127 160			255 349	322 443	407 559	513 706	648 889	806 1105	1018 1396		1543 2192	

POWER CONSIDERATIONS

(IP and Ferrite)

How large a core is needed to handle a certain amount of power? This is a question often asked, but unfortunately there is no simple answer.

There are several factors involved such as: cross sectional area of the core, core material, turns count, and of course the variables of applied voltage and operating frequency.

Overheating of the coil will usually take place long before saturation in most applications above 100 KHz. Now the question becomes ' How large a core must I have to prevent overheating at a given frequency and power level'?

Overheating can be caused by both wire and core material losses. Wire heating is affected by both DC and AC currents, while core heating is affected only by the AC content of the signal. With a normal sinewave signal above 100 KHz, both the Iron Powder and Ferrite type cores will first be affected by overheating caused by core losses, rather than saturation.

The following extrapolated AC flux density limits can be used for BOTH Iron Powder and Ferrite type cores as a guide-line to avoid excessive heating. These figures may vary slightly according to material being used.

Frequency: 100 KHz 1 MHz 7 MHz 14 MHz 28 MHz AC Flux Den. 500 gauss 150 gauss 57 gauss 42 gauss 30 gauss

Operating frequency is one of the most important factors in power capability above 100 KHz. A core that works well at 2 MHz. may burn up at 30 MHz. with the same amount of drive.

Core saturation, a secondary cause of coil failure, is affected by both AC and DC signals. Saturation will decrease the permeability of the core causing it to have impaired performance or to become inoperative. The safe operating total flux density level for most Ferrite materials is typically 2000 gauss, while Iron Powder materials can tolerate up to 5000 gauss without significant saturation effects.

Iron Powder cores (low permeability) are superior to the Ferrite material cores for high power inductors for this reason: Fewer turns will be required by the Ferrite type core for a given inductance. When the same voltage drop is applied across a decreased number of turns, the flux density will increase accordingly. In order to prevent the flux density from increasing when fewer turns are used, the flux drive will have to be decreased.

Either core material can be used for transformer applications but both will have 'trade-offs'. Ferrite type cores will require fewer turns, will give more impedance per turn and will couple better, whereas the Iron Powder cores will require more turns, will give less impedance per turn, will not couple as well but will tolerate more power and are more stable.

POWER CONSIDERATIONS (CONT)

The equation for determining the maximum flux density of a given toroidal core is as follows:

$$\label{eq:bmax} \textbf{B}_{\text{max}} = \frac{\textbf{E} \times 10^8}{4.44 \times \textbf{A}_{\textbf{e}} \times \textbf{N} \times \textbf{F}} = \frac{\textbf{E}_{\textbf{pk}}}{\textbf{A}_{\textbf{e}}} = \frac{\textbf{applied RMS volts}}{\textbf{cross-sect. area (cm}^2)} \\ \frac{\textbf{E}_{\textbf{pk}}}{\textbf{A}_{\textbf{e}}} = \frac{\textbf{applied RMS volts}}{\textbf{number of wire turns}} \\ \textbf{F} = \frac{\textbf{F}_{\textbf{pk}}}{\textbf{F}_{\textbf{e}}} = \frac{\textbf{Applied RMS volts}}{\textbf{F}_{\textbf{e}}} \\ \frac{\textbf{E}_{\textbf{pk}}}{\textbf{F}_{\textbf{e}}} \\ \frac{\textbf{E}_{\textbf{pk}}}{\textbf{F}_{\textbf{e}}} = \frac{\textbf{Applied RMS volts}}{\textbf{F}_{\textbf{e}}} \\ \frac{\textbf{E}_{\textbf{pk}}}{\textbf{F}_{\textbf{e}}} = \frac{\textbf{Applied RMS volts}}{\textbf{F}_{\textbf{e}}} \\ \frac{\textbf{E}_{\textbf{pk}}}{\textbf{F}_{\textbf{e}}} = \frac{\textbf{Applied RMS volts}}{\textbf{F}_{\textbf{e}}} \\ \frac{\textbf{E}_{\textbf{e}}}{\textbf{F}_{\textbf{e}}} = \frac{\textbf{Applied RMS volts}}{\textbf{F}_{\textbf{e}}} \\ \frac{\textbf{E}_$$

The safety factor may be increased by using the peak AC voltage in the equation. This is standard practice among many RF engineers who design broadband RF power transformers.

The above equation may be changed as shown below to make it more convenient during calculations of $B_{\mbox{\scriptsize max}}$ at radio frequencies.

$$B_{\text{max}} = \frac{E \times 10^2}{4.44 \times A_e \times N \times F} = \frac{E_{\text{pk}}}{A_e} = \frac{\text{applied RMS volts}}{\text{e cross-sect. area (cm}^2)} = \frac{E_{\text{pk}}}{N} = \frac{\text{applied RMS volts}}{\text{number of wire turns}} = \frac{1}{1000} = \frac{1}{1$$

The sample calculation below is based on a frequency of 7 MHz, a peak voltage of 25 volts and a primary winding of 15 turns. The cross-sectional area of the sample core is 0.133 cm² From previous guidelines we know that the maximum flux density at 7 MHz should be not more than 57 gauss.

$$B_{\text{max}} = \frac{25 \times 100}{4.44 \times 0.133 \times 15 \times 7} = 40.3 \text{ gauss}$$

This hypothetical toroid core will have a flux density of 40 gauss according to the above formula and when operated under the above conditions. This is well within the limits as shown above.

Temperature rise can be the result of using an undersized wire gauge for the amount of current involved as well as magnetic action within the core. Both will contribute to the overall temperature rise of the transformer. This can be calculated with the following equation:

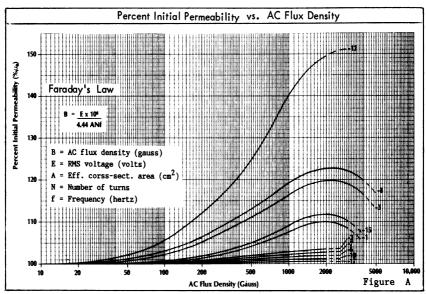
Temperature Rise (°C) =
$$\frac{\text{Total Power Dissipation (Milliwatts)}}{\text{Available Surface Area (cm²)}} \right] .833$$

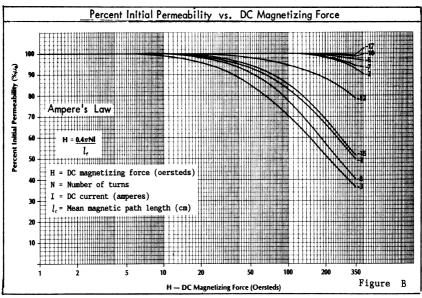
If the operating temperature (ambient temperature + temperature rise) is more than 100°C when used intermittently, or more than 75°C if used continuously, a larger size core and/or a heavier gauge wire should be selected.

Iron Powder Materials SATURATION and FLUX DENSITY

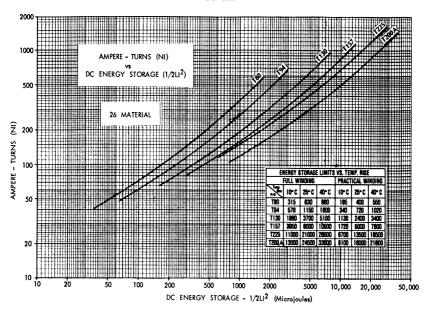
Factors affecting power capability will vary with operating conditions. Core losses are lower at low frequencies and low power levels, but increase rapidly as either is increased.

Core losses can create overheating, which in turn will affect the saturation point. Maximum flux density can be calculated with the Faraday Law and Amperes Law, both of which are shown below:



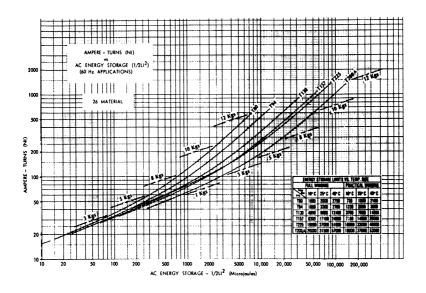


Iron Powder Toroidal Cores DC Chokes



	DC (Choke	App1	icati	lons	(single lay	er winding)	
DC Amps > Wire size >	1 Amp	2 Amps	4 Amps	6 Amps	10 Amps	15 Amps	20 Amps	30 Amps
	28 AWG	24 AWG	21 AWG	19 AWG	16 AWG	14 AWG	12 AWG	10 AWG
Part\/No								
T-37-26*	35 uh	13.5 uh	4.0 uh	1.8 uh	.8 uh	.38 uh	.16 uh	.012 uh
	41 tur	ns 27 turns	15 turns	10 turns	7 turns	5 turns	3 turns	1 turn
T-50-26*	92 uh	29.0 uh	11.3 uh	5.5 uh	2.1 uh	1.1 uh	.59 uh	.36 uh
	63 tur	ns 37 turns	25 turns	18 turns	11 turns	8 turns	6 turns	5 turns
T-80-26	380 uh	130 uh	51.3 uh	27.8 uh	11.2 uh	5.7 uh	3 uh	1.3 uh
	108 tu	rns 66 turns	45 turns	35 turns	23 turns	17 turns	12 turns	8 turns
T-94-26	650 uh 123 tu		87.5 uh 52 turns	47.2 uh 40 turns	20.0 uh 27 turns	10.2 uh 20 turns	5.3 uh 14 turns	2.6 uh 10 turns
T-130-26	1660 u	h 575 uh	231 uh	127 uh	55.0 uh	28.0 uh	16.5 uh	10.4 uh
	173 tu	rns 107 turns	75 turns	58 turns	40 turns	30 turns	23 turns	17 turns
T-157-26	3200 u	h 1100 uh	438 uh	244 uh	106 uh	55.6 uh	32 uh	16.4 uh
	213 tu	rns 122 turns	93 turns	73 turns	50 turns	38 turns	29 turns	22 turns
T-184-26*	5600 u	h 1950 uh	788 uh	439 uh	190 uh	99.6 uh	57.5 uh	29.3 uh
	213 tu	rns 122 turns	93 turns	73 turns	50 turns	38 turns	29 turns	22 turns
T-225-26	8600 u	h 2300 uh	938 uh	528 uh	230 uh	127 uh	72.5 uh	40 uh
	317 tu	rns 198 turns	139 turns	110 turns	77 turns	60 turns	46 turns	36 turns
T-300A-26*	22.4 m	h 7850 uh	3120 uh	1750 uh	760 uh	418 uh	250 uh	129 uh
	435 tu	rns 272 turns	190 turns	151 turns	105 turns	82 turns	63 turns	44 turns
T-400A-26*	51.0 m	h 17.5 mh	7120 uh	4000 uh	1760 uh	951 uh	550 uh	293 uh
	507 tu	rns 317 turns	223 turns	176 turns	122 turns	95 turns	73 turns	57 turns
Note:	* Size	not shown on	above curve	chart.	Wire size	based on M	lax. Temp. ri	ise 40°C

Iron Powder Toroidal Cores AC Line Filters

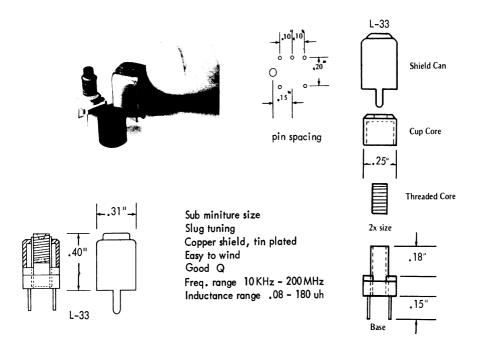


60 Hz. AC Line Filter Applications (single layer winding)

AC Amps >	1 Amp	2 Amps	4 Amps	6 Amps	10 Amps	15 Amps	20 Amps	30 Amps
Wire size >	28 AWG	24 AWG	21 AWG	19 AWG	15 AWG	13 AWG	11 AWG	9 AWG
Part\/No								
T-37 -26*	130 uh	50.0 uh	15 uh	6.7 uh	2.4 uh	1.1 uh	.60 uh	.07 uh
	41 turns	27 turns	15 turns	10 turns	6 turns	4 turns	3 turns	1 turn
T-50 -26*	460 uh	150 uh	58.8 uh	26.1 uh	9.4 uh	4.2 uh	2.4 uh	1.0 uh
	63 turns	37 turns	25 turns	17 turns	10 turns	7 turns	5 turns	3 turns
T-80 -26	1600 uh	550 uh	213 uh	94.4 uh	34.0 uh	15.1 uh	8.5 uh	3.8 uh
	108 turns	66 turns	45 turns	30 turns	18 turns	12 turns	9 turns	6 turns
T-94 -26	2899 uh	950 uh	375 uh	156 uh	56.0 uh	24.9 uh	14 uh	6.2 uh
	123 tunrs	75 turns	52 turns	33 turns	20 turns	13 turns	10 turns	7 turns
T-130 -26	7200 uhh	2500 uh	1000 uh	444 uh	160 uh	71.1 uh	40 uh	17.8 uh
	173 turns	107 turns	75 turns	50 turns	30 turns	20 turns	15 turns	10 turns
T-157 -26	13.6 mh	4650 uh	1810 uh	806 uh	290 uh	129 uhh	72.5 uh	32.2 uh
	213 turns	139 turns	93 turns	62 turns	37 turns	25 turns	18 turns	12 turns
T-184 -26*	22 mh	7750 uh	3130 uh	1390 uh	500 uh	222 uh	125 uh	56.6 uh
	213 turns	132 turns	93 turns	62 turns	37 turns	25 turns	18 turns	12 turns
T-225 -26	26 mh	9000 uh	3500 uh	1940 uh	700 uh	311 uh	175 uh	77.8 uh
	317 turns	198 turns	139 turns	110 turns	66 turns	44 turns	33 turns	22 turns
T-300A -26*	84 mh	29 mh	11.2 mh	6390 uh	2360 uh	1240 uh	750 uh	356 uh
	435 turns	272 turns	190 turns	151 turns	93 turns	72 turns	56 turns	40 turns
T-400A -26*	180 mh	61 mh	25.6 mh	14.2 mh	5300 uh	2800 uh	1650 uh	800 uh
	507 turns	317 turns	223 turns	176 turns	108 turns	83 turns	65 turns	46 turns
Note:	* Size not	shown on a	bove curve	chart.	Wire size b	ased on Max	. Temp. rise	40 ⁰ C.

Iron Powder Shielded Coil Forms Adjustable/ Slug Tuned

L-33 Coil Forms (Specify material)



Part	Frequency	A _L (uh/100t)	L ratio	Typico	al Wind	ling (mid	-freq.)
number	range (MHz)	at max L	max to min	Wire	Turns	L(uh)	Qmax
L-33-1	0.30 - 1.0	76	1.7 - 1	3/44	75	42.5	80
L-33-2	1.00 - 10.0	68	1.5 - 1	9/44	40	10.9	90
L-33-3	0.01 - 0.5	80	1.8 - 1	3/44	150	180	70
L-33-6	10.00 - 50.0	60	1.5 - 1	26	7	0.36	100
L-33-10 L-33-17		54 48	1.4 - 1 1.3 - 1	26 26	5 3	0.18 0.08	120 130

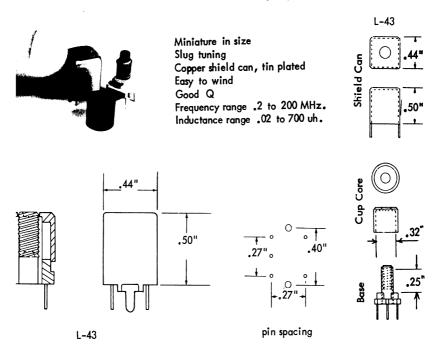
Solid magnet wire may be substituted for the Litz wire, but somewhat lower Q may result.

Most efficient when tuning slug is set at maximum L. For tuning flexibility calculate so that slug will be about 90% maximum L when at operating frequency.

$$Turns = 100 \sqrt{\frac{desired 'L' (uh)}{90\% A_L (uh/100 turns)}}$$

Iron Powder Shielded Coil Forms Adjustable/ Slug Tuned

L-43 Coil Forms (Specify material)



Part number	Frequency range (MHz)	A _L (uh/100t) at max L	L ratio max to min	Typica Wire	l Windi Turns	ing (mid L(uh)	-freq.) Qmax
L-43-1 L-43-2	0.30 - 1.0 1.00 - 10.0	115 98	1.6 - 1 1.6 - 1	5/44 9/44	149 21	230	110 120
L-43-3 L-43-6	0.01 - 0.5 10.00 - 50.0	133 85	1.8 - 1	3/44	223	600	90 130
	25.00 - 100.0 50.00 - 200.0	72 56	1.3 - 1 1.2 - 1	24 22	5 3	0.14 0.05	150 200

Solid magnet wire may be substituted for the Litz wire, but somewhat lower Q may result.

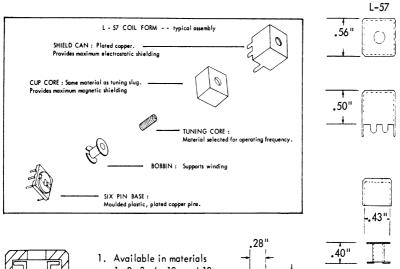
Most efficient when tuning slug is set at maximum L. For tuning flexibility calculate so that slug will be about 90% maximum L when at operating frequency.

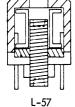
Turns =
$$100\sqrt{\frac{\text{desired 'L' (uh)}}{90\% \text{ A}_{\text{L}} \text{ (uh/100 turns)}}}$$

Iron Powder Shielded Coil Forms Adjustable/ Slug Tuned

L-57 Coil Forms (Specify material)

Part	Frequency	A _L (uh/100 t)	Color	Tuning
Number	Range	(at max. Q)	Code	Range
L-57-1	.30 MHz - 1.0 MHz	175 uh	Blue	3/1
L-57-2	1.00 MHz - 10.0 MHz	125 uh	Red	2/1
L-57-3	.01 MHz5 MHz	204 uh	Gray	3/1
L-57-6	10.00 MHz - 50.0 MHz	115 uh	Yellow	2/1
L-57-10	25.00 MHz - 100.0 MHz	100 uh	Black	2/1
L-57-17	50.00 MHz - 150.0 MHz	67 uh	Violet	1.5/1





- 1, 2, 3, 6, 10, and 12
- 2. Can be tuned from both top and bottom
- 3. Furnished with six pin base to accommodate center tapped coils.

pin spacing



Most efficient when tuning slug is set at maximum L. For tuning flexibility calculate so that slug will be about 90% maximum L when at operating frequency.

Turns =
$$100 \sqrt{\frac{\text{desired L (uh)}}{90\% \text{ A_i value (uh)}}}$$

Ferrite Cores

Ferrite Cores are available in numerous sizes and several perme-abilities. Their permeability range is from 125 to more than 5000. They are very useful for resonant circuit applications as well as wideband transformers. and they are also very useful for RFI attenuation. We can supply sizes from .23 inches to 2.4 inches in outer diameter directly from stock.

Ferrite toroidal cores are well suited for a variety of RF circuit applications and their relatively high permeability factors make them especially useful for high inductance values with a minimum number of turns, resulting in smaller component size.

There are two basic ferrite material groups: those having a permeability range from 20 to 800 mu are of the NICKEL ZINC class and those having permeabilities above 800 mu are usually of the Manganese Zinc class.

The NICKEL ZINC ferrite cores exhibit high volume resistivity, moderate stability and high 'Q' factors for the 500 KHz to 100 MHz frequency range. They are well suited for low power, high inductance resonant circuits and their permeability factors make them useful for wide band transformer applications.

The MANGANESE ZINC group of ferrites, having permeabilities from 800 mu to 5000 mu have fairly low volume resistivity and moderate saturation flux density. They can offer high 'Q' factors for the 1 KHz to 1 MHz frequency range. Cores from this group of materials are widely used for switched mode power conversion transformers operating in the 20 KHz to 100 KHz frequency range. These cores are also very useful for the attenuation of unwanted RF noise signals in the frequency range of 20 MHz. to 400 MHz and above.

A list of Ferrite toroids, including physical dimensions, magnetic properties, and the turns count formula for ferrite toroidal cores will be found on the next few pages. All items in this booklet are standard stock items and can be shipped immediately.

Ferrite Materials

MATERIAL 33 (u = 850) A manganese-zinc material having low volume resistivity. Used for low frequency antennas in the 1 KHz to 1 MHz. frequency range. Available in rod form only.

MATERIAL 43 (u = 850) High volume resistivity. For medium frequency inductors and wideband transformers up to 50 MHz. Optimum frequency attenuation from 40 MHz to 400 MHz. Available in toroidal cores. shield beads, balun cores and special shapes for RFI suppression.

MATERIAL 61 (u = 125) Offers moderate temperature stability and high 'Q' for frequencies 0.2 MHz to 15 MHz. Useful for wideband transformers to 200 MHz. and frequency attenuation above 200 MHz. Available in toroids, rods, bobbins and some two-hole baluns.

MATERIAL 63 (u = 40) For high 'Q' inductors in the 15 MHz to 25 MHz. frequency range. Available in toroidal form only.

MATERIAL 64 (u=250) Primarily a bead material having high volume resistivity. Excellent temperature stability and very good shielding properties above 400 MHz.

MATERIAL 67 (u 40) Similar to the 63 material. Has greater saturation flux density and lower volume resistivity. Very good temperature stability. For high 'Q' inductors, (10 MHz to 80 Mhz.). Wideband transformers to 200 MHz. Toroids only.

MATERIAL 68 (u = 20) High volume resistivity and excellent temperature stability. For high Q' resonant circuits 80 MHz.to 180 MHz. For high frequency inductors. Toroids only.

MATERIAL 73 (u=2500) Primarily a ferrite bead material, Has good attenuation properties from 1 MHz. through 50 MHz. Available in beads and some broadband balun cores.

MATERIAL 77 (u = 2000) Has high saturation flux density at high temperature. Low core loss in the 1 KHz to 1 MHz range. For low level power conversion and wideband transformers. Extensively used for frequency attenuation from 0.5 Mhz. to 50 MHz. Available in toroids, pot cores, E-cores, beads, broadband balun cores and sleeves. An upgrade of the former 72 material. The 72 material is still available in some sizes, but the 77 material should be used in all new design.

MATERIAL 'F' (u = 3000) High saturation flux density at high temperature. For power conversion transformers. Good frequency attenuation 0.5 MHz to 50 MHz. Toroids only.

MATERIAL 'J'/ 75 (perm 5000) Low volume resistivity & low core loss from 1 KHz.to 1 MHz. Used for pulse transformers and low level wideband transformers. Excellent frequency attenuation from 0.5 MHz to 20 MHz. Toroids and ferrite beads only.

FERRITE TOROIDAL CORES

MATERIAL 43					Permea	bility 850
0.D.	I.D.	Hgt	1	Δ		A _{I.} value
Core\/number (in)	(in)	(in)	l _e cm	$^{\mathtt{A}_{\mathbf{e}}}_{\mathtt{cm}^2}$	V _e cm ³	mh/1000 t
core(/number (III)	(111)	(111)	Citi	CIII	Cili	, 1000 c
FT-23 -43 .230	.120	.060	1.34	.021	.029	188
FT-37 -43 .375	.120	.125	2.15	.076	.163	420
	.281	.123	3.02	.133	.401	523
			3.68	.152	.559	570
FT-50A-43 .500	.312 .312	.250 .500	3.18	.303	.963	1140
FT-50B-43 .500				. 246	1.294	557
FT-82 -43 .825	.520	.250	5.26			603
FT-114-43 1.142	.750	.295	7.42	.375	2.783	952
FT-140-43 1.400	.900	.500	9.02	.806	7.270	
FT-240-43 2.400	1.40	.500	14.40	1.570	22.608	1240
MATERIAL 61					Perme	ability 125
0.D.	I.D.	Hgt	$^{1}\mathbf{e}$	A_		A _{I.} value
Core\/number (in)	(in)	(in)	-e cm	$^{\mathrm{A}}\mathrm{e}_{\mathrm{cm}^{2}}$	V _e cm ³	mh/ี/1000 t
						•
FT-23 -61 .230	.120	.060	1.34	.021	.029	24.8
FT-37 -61 .375	.187	.125	2.15	.076	.163	55.3
FT-50 -61 .500	.281	.188	3.02	.133	.401	68.0
FT-50A -61 .500	.312	.250	3.68	.152	.559	75.0
FT-50B -61 .500	.312	.500	3.18	.303	.963	150.0
FT-82 -61 .825	.520	.250	5.26	.246	1.294	73.3
FT-114 -61 1.142	.750	.295	7.42	.375	2.783	79.3
FT-114A-61 1.142	.750	.545	7.42	.690	5.120	146.0
FT-140 -61 1.400	.900	.500	9.02	.806	7.270	140.0
FT-240 -61 2.400	1.40	.500	14.40	1.570	22.608	173.0
FT-240 -61 2.400	1.40	.500	14.40	1.570	22.608	173.0
FT-240 -61 2.400	1.40	.500	14.40	1.570		
MATERIAL 63/	67			1.570	Perme	eability 40
MATERIAL 63/	67	.500 Hgt			Perme V _e	eability 40
MATERIAL 63/	67 I.D.		14.40	1.570 A _e		eability 40
MATERIAL 63/ 0.D. Core\/number (in)	67 I.D. (in)	Hgt (in)	$^{1}{ m e}$ cm	A _e cm ²	Perme V _e cm ³	eability 40 A _L value mh/1000 t
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230	67 I.D. (in)	Hgt (in) .060	1 _e cm 1.34	A _e cm ²	Perme V _e cm ³	A _L value mh/1000 t
MATERIAL 63/ 0.D. Core\number (in) FT-23 -63/67 .230 FT-37 -63/67 .375	I.D. (in) .120 .187	Hgt (in) .060 .125	1 _e cm 1.34 2.15	A _e cm ² .021 .076	Perme V _e cm ³ .029 .163	A _L value mh/1000 t 7.8 17.7
MATERIAL 63/ 0.D. Core\number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500	I.D. (in) .120 .187 .281	Hgt (in) .060 .125 .188	1 _e cm 1.34 2.15 3.02	A _e cm ² .021 .076 .133	Perme V _e cm ³ .029 .163 .401	Pability 40 A _L value mh/1000 t 7.8 17.7 22.0
MATERIAL 63/ 0.D. Core\number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50A-63/67 .500	I.D. (in) .120 .187 .281	Hgt (in) .060 .125 .188	1 _e cm 1.34 2.15 3.02 3.68	A _e cm ² .021 .076 .133	Perme V _e cm ³ .029 .163 .401	A _L value mh/1000 t 7.8 17.7 22.0 24.0
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50A-63/67 .500 FT-50B-63/67 .500	1.D. (in) .120 .187 .281 .312	Hgt (in) .060 .125 .188 .250	1 _e cm 1.34 2.15 3.02 3.68 3.18	.021 .076 .133 .152	Perme V _e cm ³ .029 .163 .401 .559	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0
MATERIAL 6.3 / 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-508-63/67 .500 FT-508-63/67 .500 FT-82 -63/67 .825	. I.D. (in) .120 .187 .281 .312 .312	Hgt (in) .060 .125 .188 .250 .500	1 _e cm 1.34 2.15 3.02 3.68 3.18 5.26	Ae cm ² .021 .076 .133 .152 .303 .246	Perme V _e , cm ³ .029 .163 .401 .559 .963 1.294	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142	. I.D. (in) .120 .187 .281 .312 .312 .520	Hgt (in) .060 .125 .188 .250 .500 .250	1.34 2.15 3.02 3.68 3.18 5.26 7.42	Ae cm ² .021 .076 .133 .152 .303 .246	Perme V _e cm ³ .029 .163 .401 .559 .963 1.294 2.783	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900	Hgt (in) .060 .125 .188 .250 .500 .250	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806	Perme V _e 3 .029 .163 .401 .559 .963 1.294 2.783 7.270	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142	. I.D. (in) .120 .187 .281 .312 .312 .520	Hgt (in) .060 .125 .188 .250 .500 .250	1.34 2.15 3.02 3.68 3.18 5.26 7.42	Ae cm ² .021 .076 .133 .152 .303 .246	Perme V _e cm ³ .029 .163 .401 .559 .963 1.294 2.783	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900	Hgt (in) .060 .125 .188 .250 .500 .250	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806	Perme V _e 3 .029 .163 .401 .559 .963 1.294 2.783 7.270	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900	Hgt (in) .060 .125 .188 .250 .500 .250	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806	Perme Ve. cm ³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0
MATERIAL 0.D. 0.D. 0.D. 0.D. 0.D. 0.D. 0.D. 0.D	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900	Hgt (in) .060 .125 .188 .250 .500 .250	1 e cm 1 · 34 2 · 15 3 · 02 3 · 68 3 · 18 5 · 26 7 · 42 9 · 02 14 · 40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Ve cm ³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608	AL value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50A-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900 1.400	Hgt (in) .060 .125 .188 .250 .500 .255 .500 .295 .500	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806	Perme Ve. cm ³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 meability 20 A _L value
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50A-63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D.	. I.D. (in) .120 .187 .281 .312 .520 .750 .900 1.400	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Ve cm ³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 meability 20 A _L value
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50A-63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D.	. I.D. (in) .120 .187 .281 .312 .520 .750 .900 1.400	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Ve cm ³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 meability 20 A _L value
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D. Core\/number (in)	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900 1.400	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Venues 163 .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 meability 20 A _L value mh/1000 t
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-508-63/67 .500 FT-508-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D. Core\/number (in) FT-23 -68 .230	1.D. (in) .120 .187 .281 .312 .312 .520 .750 .900 1.400	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Ve cm³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608 Perm Ve cm³ .029	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 Meability 20 A _L value mh/1000 t
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-508-63/67 .500 FT-508-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D. Core\/number (in) FT-23 -68 .230 FT-37 -68 .375	1.D. (in) .120 .187 .281 .312 .520 .750 .900 1.400 I.D. (in) .120 .187	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Ve. cm³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608 Perm Ve. cm³ .029 .163	A _L value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 Meability 20 A _L value mh/1000 t
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .375 FT-50 -63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .500 FT-82 -63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D. Core\/number (in) FT-23 -68 .230 FT-37 -68 .375 FT-50 -68 .500	1.D. (in) .120 .187 .281 .312 .520 .750 .900 1.400 I.D. (in) .120 .187 .281	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500 Hgt (in) .060 .125 .188	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570	Perme Ve. cm³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608 Perm Ve. cm³ .029 .163 .401	AL value mh/1000 t 7.8 17.7 22.0 24.0 24.0 22.4 25.4 45.0 53.0 meability 20 AL value mh/1000 t 4.0 8.8 11.0
MATERIAL 63/ 0.D. Core\/number (in) FT-23 -63/67 .230 FT-37 -63/67 .500 FT-50A-63/67 .500 FT-50B-63/67 .500 FT-50B-63/67 .825 FT-114-63/67 1.142 FT-140- /67 1.400 FT-240- /67 2.400 MATERIAL 68 0.D. Core\/number (in) FT-23 -68 .230 FT-37 -68 .375 FT-50 -68 .500 FT-50A-68 .500	1.D. (in) 1.20 1.87 2.281 312 520 750 900 1.400 I.D. (in) 1.20 1.87 2.281 312	Hgt (in) .060 .125 .188 .250 .500 .250 .295 .500 .500 .500 Hgt (in) .060 .125 .188 .250	1.34 2.15 3.02 3.68 3.18 5.26 7.42 9.02 14.40 1ecm 1.34 2.15 3.02 3.68	Ae cm ² .021 .076 .133 .152 .303 .246 .375 .806 1.570 Ae cm ²	Perme Ve, cm ³ .029 .163 .401 .559 .963 1.294 2.783 7.270 22,608 Perm Ve, cm ³ .029 .163 .401	AL value mh/1000 t 7.8 17.7 22.0 24.0 48.0 22.4 25.4 45.0 53.0 Meability 20 AL value mh/1000 t 4.0 8.8 11.0 12.0

FERRITE TOROIDAL CORES

	77 (72)				Permeal	ility 2000
	D.D. I.D.	Hgt	$^{ m l}_{ m e}$	$^{\mathrm{A}}_{\mathbf{e}_{2}}$ cm 2	v_{e_2}	A_L value
Core\/number	(in) (in)	(in)	cm	cm ²	cm ³	mh∕1000 t
FT-23 -77 .2	230 .120	.060	1.34	.021	.029	396
FT-37 -77 .3	375 .187	.125	2.15	.076	.163	884
FT-50 -77 .5	.281	.188	3.02	.133	.401	1100
FT-50A -77 .5	.312	.250	3.68	.152	.559	1200
	.312	.500	3.18	.303	.963	2400
	325 .520	.250	5.26	.246	1.294	1170
FT-114 -77 1.		.295	7.42	.375	2.783	1270
	142 .750	.545	7.42	.690	5.120	2340
FT-140 -77 1.4		.500	9.02	.806	7.270	2250
FT-240 -77 2.4	400 1.400	.500	14.40	1.570	22.608	3130
	'F '				Permeal	oility 3000
	D.D. I.D.	Hgt	$^{1}\mathrm{e}$	$^{A}e_{2}$	V _e	A_{I} value
Core\/number ((in) (in)	(in)	cm	cm ²	cm ³	mh/1000 t
a						
	370 .540	.500	5.42	.315	1.710	3700
FT-114 -F 1.1		.295	7.42	.375	2.783	1902
FT-150 -F 1.5		.250	8.30	.591	4.905	2640
FT-150A-F 1.5		.500	8.30	1.110	9.213	5020
FT-193 -F 1.9		.625	12.31	1.360	16.742	3640
FT-193A-F 1.9	932 1.250	.750	12.31	1.620	19.942	4460
	'J'(75)					ility 5000
	D.D. I.D.	Hgt	^{1}e	$\frac{A_{\mathbf{e}}}{cm^2}$	$v_{\mathbf{e_3}}$	A _{I.} value
Core\/number ((in) (in)	(in)	cm	cm^2	cm ³	mh√1000 t
	230 .120	.060	1.34	.021	.029	990
	375 .187	.125	2.15	.076	.163	2110
	.281	.188	3.02	.133	.401	2750
	.312	.250	3.68	.152	.559	2990
	370 .540	.250	5.42	.250	1.360	3020
	370 .540	.500	5.42	.315	1.710	6040
FT-114 -J 1.1		.295	7.42	.375	2.783	3170
FT-140 -J 1.4		.500	9.02	.806	7.270	6736
FT-150 -J 1.5		.250	8.30	.591	4.905	4400
FT-150A-J 1.5		.500	8.30	1.110	9.213	8370
FT-193 -J 1.5		.625	12.31	1.360	16.742	6065
FT-193A-J 1.9		.750	12.31	1.620	19 942	7435
FT-240 -J 2.4	1.400	.500	14.40	1.570	22.608	6845

The following equations are useful for calculating the number of turns, the inductance or the ${\tt A}_L$ value of any Ferrite toroidal core. Each core has been assigned its own ${\tt A}_L$ value which is found in the preceding Ferrite toroidal core charts.

$$N = 1000 \sqrt{\frac{\text{desired 'L' (mh)}}{A_L \text{ (mh/1000 turns)}}} \qquad L \text{ (mh)} = \frac{A_L \times N^2}{1,000,000} \qquad A_L \text{ (mh/1000 turns)} = \frac{1,000,000 \times 'L' \text{ (mh)}}{N^2}$$

$$N = \text{number of turns} \qquad L = \text{inductance (mh)} \qquad A_L = \text{inductance index (mh/1000 turns)}$$

	FI	ERRI	TE	TOR	OIDA	AL.	CORI	ES		
Phys	ical	L Di	mens	sion	s -	Fer	rite	э То	roi	ls
core\size	OD inche	s	ID inches	Hg inc	t Me hes	an leng cm	th Cros	s Sect cm ²	Volu c	me m ³
FT-23 FT-37 FT-50 FT-50 -A FT-50 -B FT-87 -FT-87 FT-87 -A FT-114 FT-114 -A FT-140 FT-150 -A FT-193 -A FT-240	.230 .375 .500 .500 .825 .870 .870 1.142 1.142 1.500 1.500 1.500 1.932 2.400	1 1 1 1	.120 .187 .281 .312 .512 .540 .750 .750 .750 .750 .750 .750 .750 .250 .250	.06 .12 .18 .25 .50 .25 .25 .50 .50 .50 .50 .62	0 5.5 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.34 2.15 3.02 3.18 5.26 5.41 7.42 7.42 9.02 8.30 2.31 4.40	1.	021 076 133 152 303 246 261 375 690 896 110 360 570	.029 .163 .401 .596 .1.294 1.712 2.783 5.120 -7.270 -4.905 9.211 16.742 119.942	
L Yo		e part nu	mber add		er to cor	e size be			oid	s
Material > 2 core size u=8		1 63 25 u=2	50 u=	7 68 40 u=2	72 20 u=200	75 00 u=50	77 000 u=2		F =3000 ι	J 1=5000
	20 55 23 68 70 150 57 73 4 NA 03 79 4 146 52 140 4 NA NA NA NA NA NA NA NA NA NA NA NA NA N	3.3 22. NA NA 0.3 25. 0.0 NA 0.0 45. NA NA NA	7 17 0 22 0 24 0 48 4 22 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	.8 4. .7 8. .0 11. .0 12. .4 11. A NAA .4 12. IA NAA IA NAAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA NAAA IA N	8 884 0 1100 0 1200 7 1170 A NA NA NA 2 2340 A NA NA NA NA NA	221 275 275 299 1 N/ 302 N/ N/ 1 N/ 1 N	0 79 0 99 0 108 108 108 108 108 108 108 108	00 00 00 00 00 00 00 10 10 10 10 10 10 1	NA NA NA NA NA 180 3700 1902 NA NA 2020 3640 4460 NA	NA NA NA NA NA 3020 6040 NA 6736 4400 8370 6065 7435 6845
Magnet	ic	Prop	ert	ies	- F	erri	te 1	Mate	ria	ls
Material >	43	61	63	67	68	72	75	77	F	J
Initial Perm.	850	125	40	40	20	2000	5000	2000	3000	5000
Max Perm. Max Flux den.	3000 2750	450 2350	125 1850	125 3000	40 2000	3500 3500	8000 3900	6000 4600	4300 4700	9500 4300
A oer, gauss Residual flux density, gauss	1200	1200	750	1000	1000	1500	1250	1150	900	500
Vol. Resist. ohms/cm	1x10 ⁵	1x10 ⁸	1x10 ⁸	1x10 ⁷	1x10 ⁷	1x10 ²	5x10 ²	1x10 ²	1x10 ²	1x10 ²
Temp. Co-eff. 20-70 deg. C	1%	.15%	.10%	.13%	.06%	.60%	.90%	.60%	.25%	. 4%
Curie Temp. C	130	350	450	500	450	150	160	200	250	140
Resonant Cir. Freq. MHz	.01 to 1 MHz	.2 to 10 MHz	15 to 25 MHz	10 to 80 MHz	80 to 180 MH:	ł	.001- 1 MHz	.001- 1 MHz	.001- 1 MHz	.001- 1 MHz
Wideband Freq. MHz. *	1 to 50 MHz	10 to 200	25 to 200	50 to 500	200- 1000	.5 to 30 MH	.2 to 15 MHz	.5 to 30 MHz	.5 to 30 MHz	1 to 15 MHz

^{1&}lt;sub>50</sub> * Based on low power, small core application. Listed frequencies will be lower with higher power.

1000-5000

1 -50 ·5-20

1 -50

.5 20

350-1500

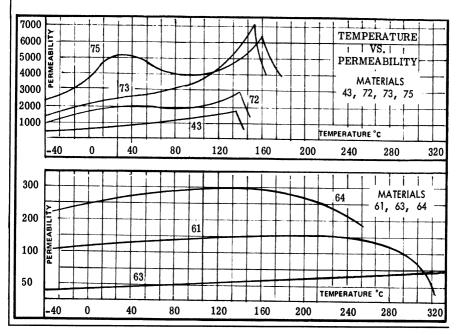
200-1000

20-600

Attenuation RF Noise, MHz

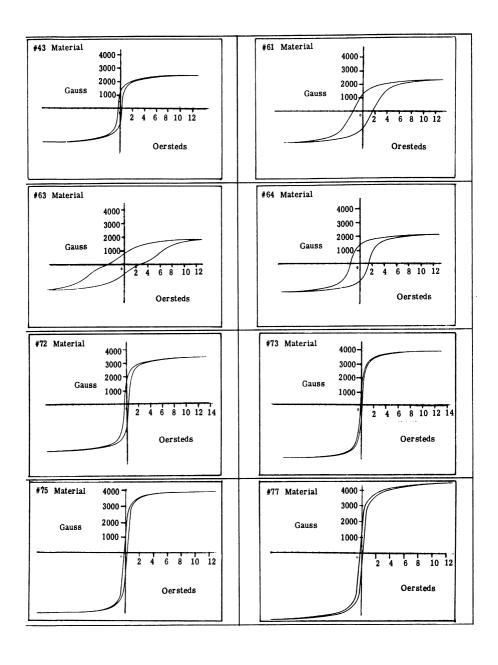
500-2000





	Ferrite				core s		si	size v		s. W		ire t		urns		
Awg wire Core\/No		12	14	16	18	20	22	24	26	28	30	32	34	36	38	40
FT-23 FT-37 FT-50	0 0 2	0 0 4	0 2 7	0 4	2 7	4 11	7 15	11 21	15 28	21 36	28 48	37 61	48 79	62 100	79 127	101 161
FT-50 -A	_	5	8	10	14 19	19 22	26 30	34 39	45 51	58 66	75 84	95 106	121	154 171	194 216	245 273
FT-50 -B FT-82	3	5 13	8 18	13 22	19 32	22 41	30 53	39 69	51 88	65 112	84 143	106 180	135 228	171 288	216 362	273 ¹ 456
FT-87A FT-114 FT-114-A	10 16 16	14 22 22	19 29 29	25 38 38	34 49 49	43 63 63	56 80 80	72 100 100	92 131 131	118 166 166	150 211 211	188 263 263	239 334 334	302 420 420	374 527 527	478 665 665
FT-140 FT-150 FT-150-A	20 16 16	27 22 22	36 29 29	42 38 38	60 49 49	77 63 63	97 80 80	125 100 100	158 131 131	201 166 166	255 211 211	318 263 263	403 334 334	507 420 420	636 527 527	801 665 665
FT-193 FT-193-A FT-240	31 31 36	41 41 46	53 53 60	68 68 77	86 86 98	109 109 123	139 139 156	176 176 198	223 223 250	282 282 317	357 357 400	445 445 499	562 562 631	707 707 793	886 886 993	1115 1115 1250
Approximate number of turns for full single layer winding on Ferrite Toroids.																

FERRITE MATERIAL HYSTERESIS LOOPS



Inductance-Turns Chart, Ferrite Toroids

MATER	IAL	#43											
turns count >		10	20	30	40	50	60	70	80	90	100		
core\/number	$\mathtt{A_L} \star$	10		30			•			,,	100		
	L		ind	luctance	in m	illihenr	ies						
FT-23 -43	188	.018		.169		.470	.677	.921	1.20	1.52	1.88		
FT-37 -43	420	.042	.168	.378		1.05	1.51	2.06	2.69	3.40	4.20		
FT-50 -43	523	.052		.471	.836	1.30	1.88	2.56	3.35		5.23		
FT-50A -43	570	.057	.228	.513	.912	1.43	2.05	2.79	3.65		5.70		
FT-50B -43	1140	.110	.456	1.03	1.82	2.85	4.10	5.59	7.30	9.23	11.4		
FT-82 -43	557	.056	.224	.503	.894	1.40	2.01	2.74	3.58		5.59		
FT-114 -43	603	.060	.241	.543	.965	1.51	2.17	2.95	3.86	4.88	6.03		
FT-140 -43	953	.095	.380	.857	1.52	2.38	3.43	4.66	6.09	7.71	9.52		
FT-23 -43 FT-37 -43 FT-50 -43 FT-50B -43 FT-82 -43 FT-114 -43 FT-140 -43 FT-240 -43	1239	.123	.494	1.11	1.97	3.09	4.44	6.05	7.90	9.96	12.3		
MATERIAL #61													
turns count >		10	20	30	40	50	60	70	80	90	100		
core\/number	A _{T.} *												
				luctance									
FT-23 -61	24.8			.022		.063		.122	.159	.201	.248		
FT-37 -61	55.3	.006	.022	.050			.199	.271			.553		
FT-50 -61	68.8	.007	.028	.062				.337			.688		
FT-50A -61	75.0 150.0 73.3 79.3	.008	.030	.068				.366	.480		.750		
FT-50B -61	150.0	.015	.060	.135				.735		1.22	1.50		
FT-82 -61	73.3	.007	.029	.066			.264	.359					
FT-114 -61	79.3	.008	.032	.071				.389					
FT-114A-61	146.0	.015	.058	.131				.715	.934				
FT-114 -61 FT-114A-61 FT-140 -61 FT-240 -61	140.0	.014	.056	.126					.896		1.40		
FT-240 -61	171.0	.007 .008 .015 .007 .008 .015 .014	.068	.154	.274	.428	.616	.838	1.09	1.39	1.71		
MATERIA	A.T. 44												
MAIERIA													
turns count >		10	20	30	40	50	60	70	80	90	100		
core\/number	$^{\mathtt{A}_{\mathtt{L}}}\!^{\star}$												
			ind	ductance									
FT-23 -63/67	7.9		.003	.007		.020		.038	.051		.079		
FT-37 -63/67	19.7	.002	.008	.018		.049		.097		.160	.197		
FT-50 -63/6/	22.0	.002	.009	.020				.108			.220		
FT-23 -63/67 FT-37 -63/67 FT-50 -63/67 FT-50A-63/67 FT-50B-63/67 FT-82 -63/67 FT-114-63/67	24.0	.002	.020	.033		.060		.112					
FT-50B-63/6/	48.0	.005	.019	.043		.120		.235					
FT-82 -63/6/	22.4	.002	.009	.020					.143				
FT-114-03/0/	25.4	.003	.010	.023		.064		.124					
FT-140-63/67 FT-240-63/67		.005	.018	.041			.162	.220			.450 .530		
F1-240-03/07	53.0	.005	.021	.048	.084	.133	.199	.260	.339	.430	. 550		
MATERI	AT. #	68											
turns count >		10	20	30	40	50	60	70	80	90	100		
core\/number	A_{Γ_x}			_	_								
Em 22 60	, ^		in	ductance	in m	illihen	ries	020	026	022	040		
	4.0	.001	.002	.004	.006	.010	.014	.020	.026		.040		
FT-37 -68	8.8		.006	.008	.014	.022	.032	.043	.056				
FT-50 -68	11.0		.004	.010	.010	.028	.040	.054	.070				
FT-50A -68	12.0		.005	.011				.059					
FT-82 -68	11.7	.001	.005	.011				.057		.095	.117		
FT-114 -68	12.7		.005	.011	.020	.032	.046	.062	.081	.123	.127		
* $A_{ m L}$ value in mh	/1000 tu	rns											

³⁴

Inductance-Turns Chart, Ferrite Toroids

MATERIAL #77													
turns count > core\/number	A L*	10	20	30	40	50	60	70	80	90	100		
inductance in millihenries													
FT-23 -77	396	.040	.158	.356	.634	.990	1.43	1.94	2.53	3.21	3.96		
FT-37 -77	884	.088	.354	.796	1.41	2.21	3.18	4.33	5.66	7.16	8.84		
FT-50 -77	1100	.110	.440	.990	1.76	2.75	3.96	6.39	7.04	8.91	11.0		
FT-50A -77	1200	.120	.480	1.08	1.92	3.00	4.32	5.88	7.68	9.72	12.0		
FT-50B -77	2400	.240	.960	2.16	3.84	6.00	8.64	11.7	15.4	19.4	24.0		
FT-82 -77	1170	.117	.467	1.05	1.87	2.93	4.21	5.73	7.49	9.48	11.9		
FT-114 -77	1270	.127	.508	1.14	2.03	3.18	4.57	6.22	8.13	10.3	12.7		
FT-114A-77	2340	.234	.936	2.13	3.74	5.85	8.42	11.4	15.0	21.4	23,4		
FT-140 -77	2250	.225	.900	2.03	3.60	5.63	8.10	11.3	14.4	18.2	22.5		
FT-240 -77	2740	.274	1.10	2.47	4,38	6.85	9.86	13.4	17.5	22.2	27.4		
MATERIAL F													
		10	20	20	40	50	۲۵	70	00	00	100		
turns count > Core\/number	A +	10	20	30	40	50	60	70	80	90	100		
core (/ number	A_L *		in	luctance	in m	illihenr	ies						
			1110	luctance	111 111.	mein	169						
FT-87A - F	3624	.362	1.45	3.26	5.80	9.06	13.0	17.8	23.2	29.4	36.2		
FT-114 - F	1902	.190	.761	1.71	3.04	4.76	6.84	9.32	12.2	15.4	19.0		
FT-150 - F *	2640	.264	1.06	2.38	4.22	6.60	9.50	12.9	16.9	21.4	26.4		
FT-150A- F	5020	.502	2.00	4.52	8.03	12.6	18.1	24.6	32.1	40.7	50.2		
FT-193 - F *	3640	.364	1.46	3.28	5.82	9.10	13.1	17.8	23.3	29.5	36.4		
FT-193A- F	4460	.446	1.78	4.01	7.14	11.1	16.0	21.9	28.5	36.4	44.6		
MATERIAI	_ J/	75											
turns count >		10	20	30	40	50	60	70	80	90	100		
core\/number	$\mathtt{A_L} \star$												
	_		ine	luctance	in m	illihenr	ies						
FT-23 - J	980	.098	. 394	.883	1.57	2.45	3.53	4.80	6.28	7.95	9.81		
FT-37 - J	2196	.219	.878	1.98	3.51	5.49	7.90	10.8	14.1	17.8	21.9		
FT-50 - J	2715	.278	1.89	2.44	4.34	6.74	8.77	13.3	17.3	22.0	27.1		
FT-50A - J	2968	.296	1.19	2.69	4.75	7.42	10.7	14.5	19.0	24.0	29.6		
FT-87 - J	3020	.302	1.21	2.72	4.83	7.55	10.9	14.8	19.3	24.5	30.2		
FT-87A - J	6040	.604	2.42	5.44	9.66	12.6	21.7	29.6	38.7	48.9	60.4		
FT-114 - J	3170	.317	1.27	2.85	5.07	7.93	11.4	15.5	20.3	25.7	31.7		
FT-140 - J	6736	.674	2.69	6.06	10.8	16.8	24.2	33.0	43.1	54.6	67.4		
FT-150 - J	4400	.440	1.76	3.96	7.04	11.0	15.8	21.6	28.1	35.6	44.0		
FT-150A- J	8365	.837	3.35	7.53	13.4	20.9	30.1	41.0	53.5	67.8	83.7		
FT-193 - J	6065	.607	2.43	5.46	9.70	15.2	21.8	29.7	38.8	49.1	60.7		
FT-193A- J FT-240 - J	7435 6845	.743 .684	2.97 2.34	6.69 6.16	11.8 11.8	18.5 17.1	26.7 24.6	36.4 33.5	47.5 43.8	60.2 55.4	74.3 68.4		
r1-240 - J	0043	.004	4.34	0.10	11.0	1/.1	44.0	٥,٠٥	43.8	4.در	00.4		

^{* (}A_{T.} values in mh/1000 turns)

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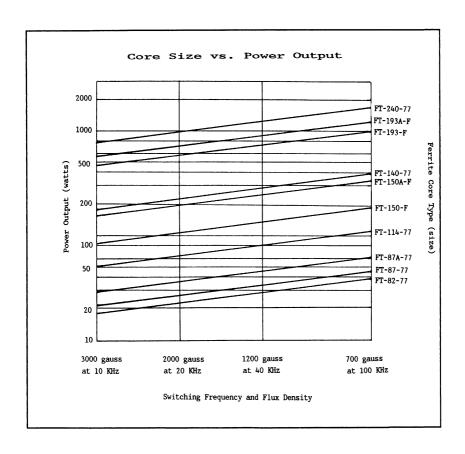
Switched Mode Power Supplies

Guide to select the proper size ferrite core

Switching power supplies require the use of high permeability Ferrite type cores, rather than high permeability Iron Powder cores. High permeability Iron Powder cores will be to lossy.

Toroidal cores may be used, however 'E' type cores are generally preferred because of greater winding ease. We stock both the Toroidal Ferrite cores and the 'E' cores in the #77 material, which is ideal for switching at frequencies of 20 KHz or higher.

See other pages in this brochure on 'E' cores for size vs. power. The chart at the bottom of this page will provide data on an approximate size toroidal core to be used for a given amount of power.



FERRITE BEADS

A Ferrite bead is a dowel-like device which has a center hole and is composed of ferromagnetic material. Ferrite beads are available in many sizes and several different ferrite materials. When a ferrite bead is placed on to a current carrying conductor it will act as an RF choke. It offers a simple, convenient, inexpensive, yet a very effective means of RF shielding, parasitic suppression and RF decoupling.

The most common noise generating suspects in high frequency circuits are power supply leads, interstage connections, and ground leads. Adjacent unshielded conductors can also provide a convenient path for the transfer of energy from one circuit to another. A few ferrite beads of the appropriate material placed onto these leads can greatly reduce or completely eliminate the problem. Best of all, they can be added to most any existing electronic circuit.

The amount of impedance is a function of both the material and the frequency, as well as the size of the bead. As the frequency increases, the permeability will decline causing the losses to rise to a peak. With a rise in frequency the bead will present a series resistance with very little reactance. Since reactance is low there is little chance of resonance which could destroy the attenuation effect. Impedance is directly proportional to the length of the bead, therefore the impedance offered by each additional bead will be additive as it is placed on to the conductor. Since the magnetic field is totally contained within the bead, it doesn't matter if the beads are touching or separated. Ferrite beads do not have to be grounded and they cannot be detuned by external magnetic fields.

We recommend the #73 or the #77 ferrite bead material for the attenuation of RFI resulting from transmissions in the amateur band. The #43 material will provide best RFI attenuation from 30 to 200 MHz, although it is still very effective for the amateur band. The #64 material is most effective above 200 MHz. and #75 material is recommended for frequencies below 10 MHz. The #75 material can also be very effective even below the AM broadcast band.

Ferrite toroidal cores can also function as frequency attenuators and the same rules will apply. In some cases a toroidal core may be more desirable since it will offer larger than one half inch ID. Not all bead materials are found in the toroidal core line. Whenever possible use the recommended bead material. If not available, substitute with a toroidal core material having the closest permeability. The lower permeability materials will have the greatest effect on the higher frequencies as will the higher permeability materials have the greatest effect on the lower frequencies.

FERRITE BEADS (cont)

A Ferrite bead is usually thought of as quite a small device with a very small ID where only one pass of the wire is practical. However, there are now up to one-half inch ID beads available for coax and larger wire bundles. Also, several turns of smaller wire may be wound on to these larger beads, in which case the impedance will increase as to the number of turns squared. The larger size beads are also available in a 'split' version for easy installation. See the following page for dimensions and part numbers.

The number of turns on a single hole Ferrite bead or a toroidal core is identified by the number of times the conductor passes through the center hole. To physically complete one turn it would be necessary to cause the wires to meet on the outside of the device, however the bead or core does not care about the termination of each end of the wire and considers each pass through the center hole as one turn. (This does not apply to multihole beads)

When winding a six-hole bead, the impedance depends upon the exact winding pattern. For instance, it can be wound clock-wise or counter clock-wise progressively from hole to hole, or criss-crossed from side to side, or each turn can be completed around the outside of the bead. Each type of winding will produce very different results. The impedance figures for the six-hole bead in our chart is based on the current industry standard, which is two and one half turns threaded through the holes, criss-crossing from one side to the other.

Fairly high currents can be tolerated before saturation begins to occur. If saturation does occur, impedance will drop to a very low level causing the bead to become ineffective as an RF attenuator. Once the cause of saturation has been removed, the bead will return to normal with no ill effects.

Temperature rise above the Curie point will also cause the bead to become non-magnetic, rendering it useless as a noise attenuating device. As soon as the cause of the temperature rise has been corrected, and the bead has been allowed to cool, normal operation will be regained and no damage will result. Depending on the material, Curie temperature can run anywhere from 120°C to 500°C. See 'Magnetic Properties' chart for specifics.

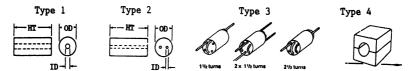
The #73 and #75 materials, as well as other very high permeability materials are semi-conductive and care should be taken not to position the cores or beads in such a manner that they would be able to short uninsulated leads together, or to ground. Other lower permeability materials with higher resistivity are non-conductive and this precaution is not necessary.

Ferrite Shielding Beads										
Part number	Bead type		sions (ID	inches) Hgt	A _L of 43	Mater: 64	ials (mh 73	n/1000 75	turns) 77	Impedance factor*
FB-()-101	1	.138	.051	.128	510	150	1500	3000		1.00
FB-()-201	1	.076	.043	.150	360	110	1100			0.70
FB-()-301	1	.138	.051	.236	1020	300	3000			2.00
FB-()-801	1_	.296	.094	. 297	1300	390	3900			2.60
FB-(64}-901	2	. 250	.050	.417		1130				7.50 **
FB-()-1801	1	.200	.062	.437	2000	590	5900			3.90
FB-()-2401	1	.380	.197	.190	520		1530			1.02
FB-()-5111	3	.236	.032	. 394	3540	1010				6.70 ***
FB-()-5621	1	.562	.250	1.125	3800				9600	6.40
FB-()-6301	1	.375	.194	.410	1100				2600	1.70
FB-(43)-1020		1.000	.500	1.112	3200					6.20
FB-(77)-1024	1	1.000	.500	.825					5600	3.70
2X-(43)-151	4	1.020	.500	1.125	Split bear	1, 43 Ma	t. Z=159	@ 25 MHz	. Z=245	@ 100 MHz
2X-(43)-251	4	.590	.250	1.125	Split bear	•				@ 100 MHz.

Notes: Complete the part number by adding material number in space (--) provided.

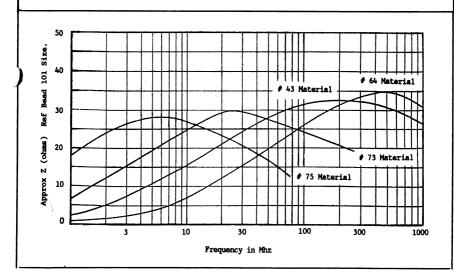
A_L values based on low frequency measurements. (mh/1000 turns) = nanohenries/turns²

*** Based on a single 'U-turn' winding. **** Based on a 2 1/2 turn, side to side winding.



Material vs Frequency vs Impedance

* Impedance Factor: The following chart is based on the '101' size bead which will be used as a reference. Impedance in ohms for a given size bead can be approximated, if the impedance of the `101' bead (from the curves) is multiplied by the impedance factor for the given bead.



Ferrites for RFI

Ferrite toroidal cores, as well as beads, can be very useful in the suppression of unwanted RF signals but we do not claim them to be a cure-all for all RFI problems. There are different types of noise sources, each of which may require a different approach. When dealing with any noise problem it is helpful to know the frequency of the interference. This is valuable when trying to determine the correct material as well as the maximum turns count.

RFI emanating from such sources as computers, flashing signs, switching devices, diathermy machines, etc. are very rich in harmonics and can create noise in the high and very high frequency regions. For this type of interference, the #43 material is probably the best choice since it has very good attenuation up to 200 MHz and better. Some noise problems may require additional filtering with hi-pass or lo-pass filters. If the noise is of the differential-mode type, an AC line filter may be required. Ferrite cores are not recommended for differential-mode noise. See section on AC line filters which use #26 Iron Powder material.

In some cases the selected core will allow only one pass of the conductor, which is considered to be one turn. In other cases it may be possible to wind several turns on to the core. When installing additional cores on the same conductor, the impedance of each core will be additive. When multiple turns are passed through a core, the impedance will increase in relation to the number of turns squared.

Keep in mind that because of the wide overlap in frequency range of the various materials, more than one material can provide acceptable results. When using toroidal cores, materials 77, and 'F' are recommended for RFI caused by amateur transmitters. We suggest not more than 15 turns for this frequency range.

The #43 material can be used to attenuate frequencies from about 2 MHz to 200 MHz with increasing attenuation as the frequency increases. It can be effective for the amateur band as well, but optimum results are above 30 MHz. Use no more than 15 turns for the amateur band and as the frequency becomes greater the turns count should gradually be reduced. For anything above 200 MHz, use a small #61 material ferrite toroidal core, or a #64 material ferrite bead. Normal practice is to make only one pass of the conductor through the core or bead. Impedance can be increased by using two or more cores or beads.

The 'J' material is recommended for frequencies below 10 MHz. but can also be very effective even below the AM broadcast band. A maximum of 30 turns is suggested.

Computers are notorious for RF radiation, especially some of the older models which were made when RFI requirements were quite minimal. RFI can radiate from inter-connecting cables, AC power cords and even from the cabinet itself. ALL of these sources must be corrected before complete satisfaction can be achieved.

FERRITES FOR RFI (cont)

First, examine the computer cabinet to make sure that good shielding and grounding practices have been followed. If not, do what you can to correct it. If you suspect that RF is feeding back into the AC power system from your computer, wrap the power cord through an FT-240-43 or an FT-240-77 toroidal core, not more than 15 times. The power cord plug will probably limit the number of turns and fewer will be OK. This will act as an RF choke on the power cord and should prevent RF from feeding back into the power system where it can affect other electronic devices which may be connected to the same power source.

Split ferrite beads, cores and bars are now available for ease of installation without removing the end connector of the cable. The split beads and sleeves are useful for wire bundles and coax cables. (2X-43-251 for quarter inch ID and the 2X-43-151 for half inch ID) Usually, only one pass of a conductor through a split core is practical or desirable.

Split bars are especially designed for computer flat ribbon cables. Use the 2X-43-051 for a 2.5" width cable, the 2X-43-951 for the 2" width, and the 2X-43-651 for the 1.3" width cable. Two or more cores can be placed on the same cable, in which case the impedance will be additive.

It is possible for an unwanted RF signal to enter a piece of equipment by more than one path, If so, ALL of these paths must be blocked before there will be noticeable effect. Don't overlook the fact that RFI may be entering the equipment by radiation directly from an amateur antenna feed line, usually due to a mismatch causing high SWR and RF radiation. This, of course, can be checked with an SWR meter, and can be corrected by installing an antenna balun, or by placing three or four ferrite beads over the coax at the antenna feed point.

Use the FB-77-1040 bead for the half inch OD coax, (see above for split version) or the FB-77-5621 bead for quarter inch OD (again see above for split version). This should prevent RF reflection back into the outside shield of the coax feed line, which could radiate RFI and TVI

RFI in telephones can be substantially reduced with the insertion of an RF choke in each side of the talk circuit (red and green wires). An FT-50A-75 core with about 20 turns of enamelled wire will make an excellent one millihenry choke for this purpose. These can be located inside the phone base out of sight. If mounting inside the phone base is not possible because of lack of space, these chokes may be placed in a tiny plastic box and mounted near the wall jack. If this sounds like to much work, similar results can be obtained by winding several turns of the telephone wall-cord through a ferrite FT-140-77 core. For frequencies below the amateur band use the F-140-J core.

FERRITE CORES FOR RFI SUPPRESSION

Following is a list of a few of the larger Ferrite Beads (FB), Ferrite Toroidal Cores (FT), and Split Ferrite Cores (2X), all of which are extensively used for RFI problems involving multiple wire bundles, coaxial cables, microphone cables, AC power cords, telephone cables, computer cables, etc.

The 43 material is a good all around material for most RFI problems. However the lower frequencies from .5 to 10 MHz. can best be served with the 'J' or 75 material. The 77 material can provide excellent attenuation of RFI caused by amateur radio frequencies from 2 to 30 MHz. and the 43 material is best for everything above 30 MHz. however, it is still very effective across the entire amateur band but not quite as good as the 77 material. The 73 material is specifically a small ferrite bead material having a permeability of 2500 and can provide RF attenuation very similar to the 77 ferrite core material.

When a number cores are strung on the same conductor, the total impedance will be the sum impedance of all cores. When a conductor is passed through the center hole of a toroidal core a number of times, the impedance will increase in proportion to the number of turns squared.

Split beads and bars (2X) are now available and can be installed without removing the end connector from the cable. Split bars are especially designed for computer ribbon cables. They are presently available for 1.3", 2.0" and 2.5" computer ribbon cables. For greater attenuation use additional cores.

Below are a few of the most widely used cores for RFI, showing typical $^{\prime}Z^{\prime}$ in ohms for one turn at 25 MHz and 100 MHz. Most sizes are available in 43, and 77 materials. Those sizes available in the J material are marked with *

	Part number	A dim. (in)	B dim. (in)	C dim. (in)	25 MHz	100 MHz	
	* FT-50A-75 FT-50B-43 FT-50B-77 * FT-87A-75 * FT-114-43 FT-114-77 * FT-140-43 FT-140-77 * FT-193- J * FT-240-43 FT-240-77	.500 .500 .500 .870 1.142 1.142 1.400 1.400 1.930 2.400 2.400	.312 .312 .312 .540 .750 .750 .900 .900 1.250 1.400	.250 .500 .500 .500 .295 .295 .500 .500 .625 .500	below 56 74 below 27 35 47 62 below 58 76	10 MHz 90 60 10 MHz 47 29 75 50 10 MHz 108 66	
	2X-43-251 2X-43-151	.590 1.020	.250 .500	1.125. 1.125	171 159	275 245	
# O	FB-43-1020 FB-77-1024 FB-43-5621 FB-77-5621 FB-43-6301 FB-77-6301	1.000 1.000 .562 .562 .375 .375	.500 .500 .250 .250 .194 .194	1.120 .825 1.125 1.125 .410 .410	155 166 171 270 55 73	235 135 250 215 48 59	
	2X-43-651 2X-43-951 2X-43-051	for 2.0	3" ribbor)" ribbor 5" ribbor	cable	97 105 90	200 285 250	

Broadband Transformers

Broadband Transformers, as the name implies, are transformers which will operate over a broad frequency range. They can provide a step-up or a step-down impedance ratio, match an unbalanced source to a balanced load, or serve both purposes.

The two-hole, 'binocular type', ferrite core, known as the balun core, is very popular for low power applications. Balun cores will provide maximum impedance per length of turn which will better serve the broadband transformer. Two-hole balun cores are widely used as 75 and 300 ohm matching transformers for receivers and low power UHF and VHF applications.

The bandwidth of a broadband transformer has limitations. The functions which control the low frequency performance are parallel inductance and parallel resistance. This combination must remain sufficiently high in order to maintain an acceptable match. Unless a very low 'Q' core is used these will be the dominant factors. Normally, the inductive reactance at the lowest frequency should be four times greater than the source impedance. However, in order to achieve this ratio, we may find that excessive turns may be required which will adversely affect the high frequency performance. Using a core of high permeability will minimize the number of required turns.

The factors which limit the high frequency performance are distributed capacity and inductance leakage due to uncoupled flux. The more the distributed capacity and the flux leakage can be minimized, the better will be the high frequency performance of the transformer. The best compromise between distributed capacity and leakage inductance can be obtained by twisting the conductors together prior to winding. This greatly minimizes the leakage inductance in small transformers.

In applications which generate minimal flux, such as in low power applications and 1 to 1 ratio transformers, the goals can best be accomplished by using a high permeability core to minimize turns at the lowest frequency. Fewer turns will create less distributed capacity which will improve the high frequency response.

Generally, ferrite cores are preferred for broadband transformers because of their high permeability factors. However, in power applications the high permeability ferrite cores can be easily saturated, and care must be taken to keep the induced flux density well below the maximum flux density rating of the core in order to confine the signal energy to the linear portion of the flux density curve. Detailed information can be found in the 'Ferro- magnetic Design and Applications Handbook' by Doug DeMaw. We now stock this item.

The main concern in power applications is core loss generated by the net induced flux. In this case, iron powder cores are usually preferred because of their higher maximum flux density rating. Core loss increases at a squared rate with flux density at any given frequency.

BALUNS and WIDEBAND CORES

The two-hole balun is commonly used for wideband transformers and impedance matching devices. The primary concern, when designing a wideband transformer, is to extend the banddwidth with a minimum of loss. The limiting factors are inductive reactance and core loss.

By winding through both holes of the binocular type two hole balun, a higher inductance per turn can be obtained than would otherwise be possible with a single hole core.

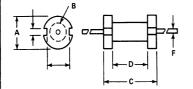


Dimensions in inches; $A_{\overline{L}}$ value in mh/1000 turns based on hole to hole winding

Part No.	OD	ID	Hgt	Th	Type	$^{\mathtt{A}}_{\mathtt{L}}$	Part No.	OD	ID	Hgt	Th	Type	$^{\mathtt{A}}_{\mathtt{L}}$
BN-43-202	.525	.150	.550	.295	one	2890	BN-61-2302	.136	.035	.093	.080	one	100
BN-43-2302	.136	.035	.093	.080	one	680	BN-61-2402	.280	.070	.240	.160	one	280
BN-43-2402	.280	.070	.240	.160	one	1277	BN-61-1702	.250	.050	.470		two	420
BN-43-3312	.765	.187	1.000	.375	one	5400	BN-61-1802						310
BN-43-7051	1.130	.250	1.130	.560	one	6000	BN-73-202						8500
BN-61-202	.525	.150	.550	.295	one	425	BN-73-2402	.275	.070	.240	.160	one	3750

Ferrite Bobbin Cores

Ferrite bobbins provide a convenient means of winding RF chokes. Because of their open magnetic path, they can handle more current than toroids of similar To aid in the design of such chokes, we have provided AL values, a winding table, and ampere-turn ratings for each bobbin.



DIMENSIONS

37

38

В

.11

.08

BOBBIN

part number

5.0 mh

10.0 mh

542

762

Winding table: number of turns to completely fill bobbin.

20 22 24 26 28 32 9 14 23 35 56 164 205 400 B-72-1111 20 22 24 26 28 30 32 34 36 wire size B-72-1011 24 39 60 93 148 230 425 535 1050

F

506

D

10.0 mh

25.0 mh

A_L value in mh/1000 turns

34

NI

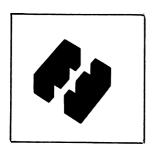
.25

.16

A_L 17 .107" #22 Bobbin # B-72-1111 .196" . 500" .400" 60 Bobb in # B-72-1011 .500" #20 39 130 .187" .750" .372" A_L= 17 BOBBIN # B-72-1011 A_L= 39 NI = 130 BOBBIN # B-72-1111 NI= 60 Inductance wire turns wire size I (max) Inductance wire turns wire size l (max) 25 uh 25 20 5.20 10 uh 24 24 2.50 50 uh 36 22 3.60 1.60 25 uh 38 26 100 uh 50 24 2.60 1.10 50 uh 54 28 250 uh 80 26 1,60 .78 100 uh 77 30 500 uh 113 27 1,10 121 31 .50 250 uh 1.0 mh .80 160 28 .35 500 uh 171 32 .50 2.5 mh 253 30 34 .25 1.0 mh 243 358 32 .36 383 36 .16 5.0 mh 2,5 mh

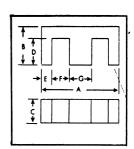
С

FERRITE 'E' CORES



TYPE 77 FERRITE MATERIAL permeability 2000

These cores are ideally suited for low power applications up to 200 watts. A nylon bobbin is supplied for easy winding.



E-Core Physical Dimensions (inches)

Part No.	A	В	С	D	E	F	G	Power
EA-77-188	.760	.318	.187	.225	.093	.192	.187	10 watts
EA-77-250	1.000	.380	.250	.255	.125	.250	.250	20 watts
EA-77-375	1.375	.562	.375	.375	.187	.312	.375	70 watts
EA-77-500	1.625	.650	.500	.405	.250	.312	.500	100 watts
EA-77-625	1.680	.825	.605	.593	.234	.375	.468	200 watts

E-Core Magnetic Properties

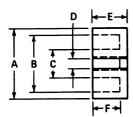
Part No.	A _e mm²	I _e mm	Ve mm ³	A _s mm ²	A _w mm ²	A _C x A _W m	A _L value h/1000 turns
E-77-188	22.5	40.1	900	1050	55.7	1250	1350
E-77-250	40.4	48.0	1930	1700	80.6	3250	1660
E-77-375	90.3	68.8	6240	3630	151.0	13700	2760
E-77-500	160.0	76.7	12300	5410	163.0	26100	4470
E-77-625	184.0	98.0	18000	7550	287.0	52900	4150

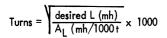
	Wire	siz	ze	vs.	. 1	lumb	er	of	tur	ns	
Part No.	18	20	22	24	26	28	30	32	34	36	38
EA-77-188	21	33	50	79	125	196	293	439	669	1046	1548
EA-77-250	34	62	93	147	232	364	532	814	1240	1938	
EA-77-375	63	94	149	235	372	582	868	1302	1984		
EA-77-500	50	141	212	335	532	829	1236	1855			
EA-77-625	159	250	375	593	939	1470	2101				

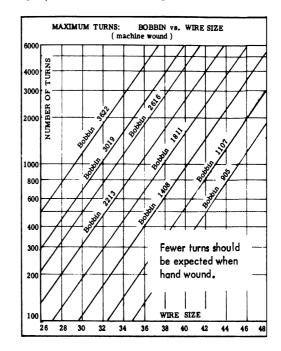
Ferrite POT Cores

Ferrite Material #77, 2000 Permeability









Physical Dimensions (In millimeters)

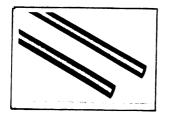
part mumber	A	В	С	D	E	F
PC-1107-77	11.10	9.20	4.60	2.10	3.21	2.27
PC-1408-77	14.05	11.80	5.90	3.10	4.18	2.90
PC-1811-77	18.00	15.25	7.45	3.10	5.27	3.70
PC-2213-77	21.60	18.70	9.25	4.55	6.70	4.70
PC-2616-77	25.50	21.60	11.30	5.55	8.05	5.60
PC-3019-77	30.00	25.40	13.30	5.55	9.40	6.60
PC-3622-77	35.60	30.40	15.90	5.55	10.85	7.40

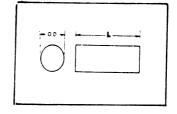
Magnetic Dimensions

part number	$^{\mathrm{A}}\mathrm{_{e}}$	$^{1}\mathbf{e}$	$v_{\mathbf{e}}$	A _{T.}	Power
	mm ²	mm	mm ³	mh/1000-t	Based on 20 KHz
PC-1107-77	15.9	15.9	252	1420	Max 3 watts
PC-1408 77	25.0	20.0	500	1960	Max 5 watts
PC-1811-77	43.0	25.9	1120	2880	Max 10 watts
PC-2213-77	63.0	31.6	2000	3660	Max 20 watts
PC-2616-77	93.0	37.2	3460	4700	Max 50 watts
PC-3019-77	136.0	45.0	6100	5900	Max 70 watts
PC-3622-77	202.0	53.0	10600	7680	Max 90 watts

Note: Power ratings are conserative, based on 20 KHz. switching frequency.

Ferrite Rods





Part number	Material	Perme- ability	Diameter (in)	Length (in)	Al value mh/1000 t	Ampere turns
R61-025-400	61	125	.25	4.0	26	110
R61-033-400	61	125	.50	4.0	32	185
R61-050-400	61	125	.50	4.0	43	575
R61-050-750	61	125	.50	7.5	49	260
R33-037-400	33	800	.37	4.0	62	290
R33-050-200	33	800	.50	2.0	51	465
R33-050-400	33	800	.50	4.0	59	300
R33-050-750	33	800	.50	7.5	70	200

FERRITE RODS are available in various sizes of both the #33 and #61 materials, which are standard stock items here at Amidon. The most common use of a ferrite rods is for antennas and choke applications.

ANTENNAS: The #61 material rods are widely used for commercial AM radio antennas and on up to 10 MHz. The #33 material rods are more suitable for the VLF frequency range.

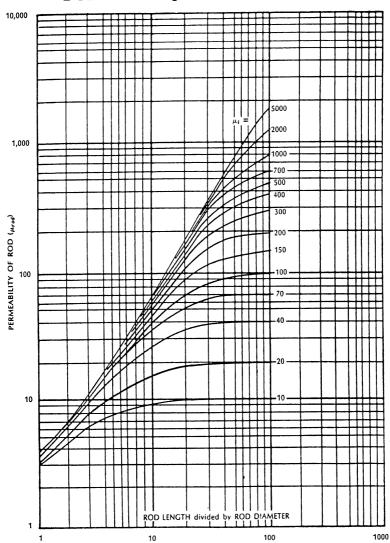
CHOKE APPLICATIONS; Both the #33 and the #61 material rods are extensively used in choke applications. The #33 material should be selected for the 40 and 80 meter bands and the #61 material is most suitable for 10 through 40 meters. The #33 material rods are also often used in speaker cross-over networks. Due to the open magnetic structure of the rod configuration, considerable current can be tolerated before it will saturate.

There are several factors that have a direct bearing on the effective permeability of a ferrite rod, which in turn will effect inductance and 'Q', as well as the $A_{\underline{L}}$ value of the rod and its ampere-turns rating. These are: (1) Length to diameter ratio of the rod, (2) Placement of the coil on the rod, (3) Spacing between turns and, (4) Air space between the coil and the rod. In some cases the effective permeability of the rod will be influenced more by a change in the length to diameter ratio than by a change in the initial permeability of the rod. At other times, just the reverse will be true.

Greatest inductance and ${\rm A_L}$ value will be obtained when the winding is centered on the rod, rather than placed at either end. The best 'Q' will be obtained when the winding covers the entire length of the rod.

Because of all of the above various conditions it is very difficult to provide workable $\rm A_L$ values, however we have attempted to provide a set of $\rm A_L$ and NI values for various types of rods in our stock. These figures are based on a closely wound coil of #22 wire, placed in the center of the rod and covering nearly the entire length. Keep in mind that there are many variables and that the inductance will vary according to winding technique.

Permeability of Ferrite Rods



PERMEABILITY OF ROD VS. ROD LENGTH DIVIDED BY ROD DIAMETER FOR VARIOUS MATERIAL PERMEABILITIES

This family of curves shows the value of the effective permeability of a ferrite rod as a function of its length to diameter ratio, as well as a function of the material permeability of the rod. It illustrates that generally, a great difference exists between the material permeability and the effective permeability of a rod. It also illustrates how, in some instances, the effective permeability of a rod can be influenced by changing its mechanical dimensions, more than by changing its material permeability, while in other cases, the reverse is true.

